# TSTE19 Power Electronics 

## Examination (TEN1)

Time: ..... Monday 25 March 2013 at $8.00-12.00$
Place: ..... U3
Responsible teacher: Kent Palmkvist, ISY, 2813 47, 0705233159 (kentp@isy.liu.se) Will visit exam location at 9 and 11.
Number of tasks: ..... 5
Number of pages: 4 (including this one)
Allowed aids: Calculator
Notes:A pass on the exam requires approximately 30 points.Remember to indicate the steps taken when solving problems.Answers may be given in Swedish and/or English.
Exam presentation: Monday 8 April 2013 12.30-13.30 (Kent Palmkvist's office)

1. a) What will be the output waveform shape of a PWM based DC-AC inverter if the controlling sinusoidal waveform is driving the inverter with maximum overmodulation?
b) Is the speed of the induction motor dependent on the amplitude or frequency of the input voltage?
c) Does a power bipolar transistor have a larger or smaller current amplication factor B compared to a small signal bipolar transistor?
d) Can the switch mode DC-AC inverter feed energy back into the voltage source?
e) What does the acronym IGBT mean?
2. The buck converter shown below is generating an output voltage $\mathrm{V}_{\mathrm{o}}=3 \mathrm{~V}$. The inductor $\mathrm{L}=18 \mu \mathrm{H}$, switching frequency $\mathrm{f}_{\mathrm{s}}=50 \mathrm{kHz}, \mathrm{C}$ is large, switching ratio $\mathrm{D}=0.1$, and the input voltage $\mathrm{V}_{\mathrm{d}}=12 \mathrm{~V}$.
a) What is the output current $\mathrm{I}_{\mathrm{o}}$ ?
b) What is the average input current $\mathrm{I}_{\mathrm{d}}$ ?
c) At what switching ratio D will the converter switch from discontinuous mode to continuous mode?

3. Assume the inductor current $\mathrm{i}_{\mathrm{L}}$ shown below is the inductor current of the buck converter above (at a different $\mathrm{D}, \mathrm{V}_{\mathrm{o}}$ and $\mathrm{I}_{0}$ setting compared to task 2). Assume the maximum ripple voltage is defined as $0.1 \mathrm{~V}, \mathrm{~T}_{\mathrm{s}}=20$ us, and that $\mathrm{i}_{\mathrm{Lmax}}=6 \mathrm{~A}$.
a) Draw the output voltage ripple on $V_{0}$.
b) What minimum size of C to keep the ripple within limits?
c) What will be the additional ripple voltage contributed by capacitors ESR if it is $0.1 \Omega$ ? (4)


4. The full-bridge rectifier shown above to the left have the source voltage vs shown above to the right. The inductor $\mathrm{L}=34 \mathrm{mH}$ and the output current $\mathrm{Io}=10 \mathrm{~A}$.
a) Draw the current is and voltages $\mathrm{v}_{\mathrm{L}}$ and vo waveforms. Indicate also when each diode is conducting or not conducting.
b) Calculate the average output voltage $\mathrm{V}_{\mathrm{o}}$.
c) What is the source displacement power factor (DPF)?

5. The snubber circuit above is designed to reduce the di/dt over the switch at turn-on. The switch have a tri of $4 \mu \mathrm{~s}$. The input voltage $\mathrm{V}_{\mathrm{d}}$ is 200 V , and the output current $\mathrm{I}_{0}$ is 10 A . The turn-on snubber shall be designed so that the switch voltage at turn on is $5 \%$ of the $\mathrm{V}_{\mathrm{d}}$ voltage, and that the switch current $I_{s w}$ is equal to $I_{0}$ after $t_{r i}$. The switching frequency is 1 kHz . Assume the snubber time constant is much larger than the transistor turn-off time.
a) Draw the waveform of the switch current isw and voltage vsw when turning on the switch turns on and when the switch turns off.
b) Calculate the value of L .
c) Assume the turn-off switch voltage $\mathrm{v}_{\mathrm{SW}}$ is not allowed to be larger than twice the value of $\mathrm{V}_{\mathrm{d}}$. What is the largest allowed value of R ?

Formula collection TSTE19 Power Electronics
Fourier series coefficients using symmetri, Table 3.1
Even

$$
f(-t)=f(t) \quad b_{h}=0 \quad a_{h}=\frac{2}{\pi} \int_{0}^{\pi} f(t) \cos (h \omega t) d(\omega t)
$$

Odd

$$
f(-t)=-f(t) \quad a_{h}=0 \quad b_{h}=\frac{2}{\pi} \int_{0}^{\pi} f(t) \sin (h \omega t) d(\omega t)
$$

Half-wave

$$
\begin{aligned}
f(t)=-f\left(t+\frac{1}{2} T\right) \quad a_{h} & =b_{h}=0 \text { for even } h \\
a_{h} & =\frac{2}{\pi} \int_{0}^{\pi} f(t) \cos (h \omega t) d(\omega t) \text { for odd } h \\
b_{h} & =\frac{2}{\pi} \int_{0}^{\pi} f(t) \sin (h \omega t) d(\omega t) \text { for odd } h
\end{aligned}
$$

Even quarter-wave Even and half-wave $b_{h}=0$ for all $h$

$$
\begin{array}{ll}
a_{h}=\frac{4}{\pi} \int_{0}^{\frac{\pi}{2}} f(t) \cos (h \omega t) d(\omega t) & \text { for odd } h \\
a_{h}=0 & \text { for even } h
\end{array}
$$

Odd quarter-wave Odd and half-wave $a_{h}=0$ for all $h$

$$
\begin{array}{ll}
b_{h}=\frac{4}{\pi} \int_{0}^{\frac{\pi}{2}} f(t) \sin (h \omega t) d(\omega t) & \text { for odd } h \\
b_{h}=0 & \text { for even } h
\end{array}
$$

Undamped series resonant circuit, equations 9-3, 9-4


Undamped parallel resonant circuit, equations 9-20, 9-21

$$
\begin{align*}
& \text { I }\left\{\mathrm{i}_{\mathrm{L}}\left[\mathrm{I}_{\mathrm{L} 0}\right]+i_{L}(t)=I_{d}+\left(I_{L 0}-I_{d}\right) \cos \omega_{0}\left(t-t_{0}\right)+\frac{V_{c 0}}{Z_{0}} \sin \omega_{0}\left(t-t_{0}\right)\right.  \tag{9-20}\\
& v_{c}(t)=Z_{0}\left(I_{d}-I_{L 0}\right) \sin \omega\left(t-t_{0}\right)+V_{c 0} \cos \omega_{0}\left(t-t_{0}\right) \tag{9-21}
\end{align*}
$$

Integration rules

$$
\begin{aligned}
& \int_{a}^{b} f(x) d x=\int_{A}^{B} f(g(t)) g^{\prime}(t) d t \quad \text { if } a=g(A), b=g(B), \text { and } g \text { is monotone in }[A, B] \\
& \int_{a}^{b} \sin (x) d x=[-\cos (x)]_{a}^{b} \\
& \int_{a}^{b} \cos (x) d x=[\sin (x)]_{a}^{b}
\end{aligned}
$$

