

TSTE19 Power Electronics

Lecture 4
Tomas Jonsson
ISY/EKS

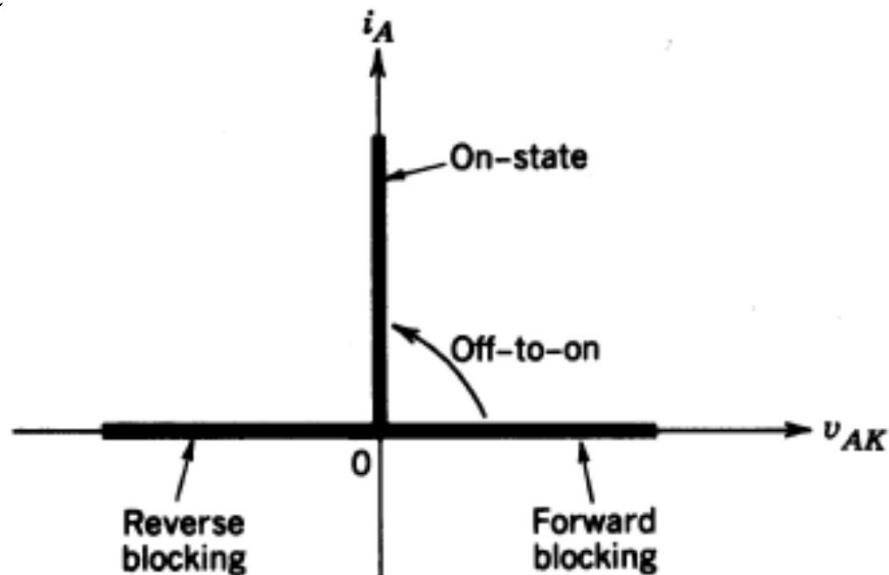
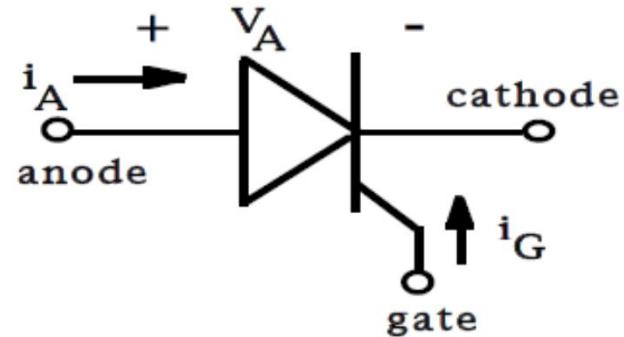
Outline

- The thyristor
- Controlled rectifier and inverters
 - Single phase
 - Three phase

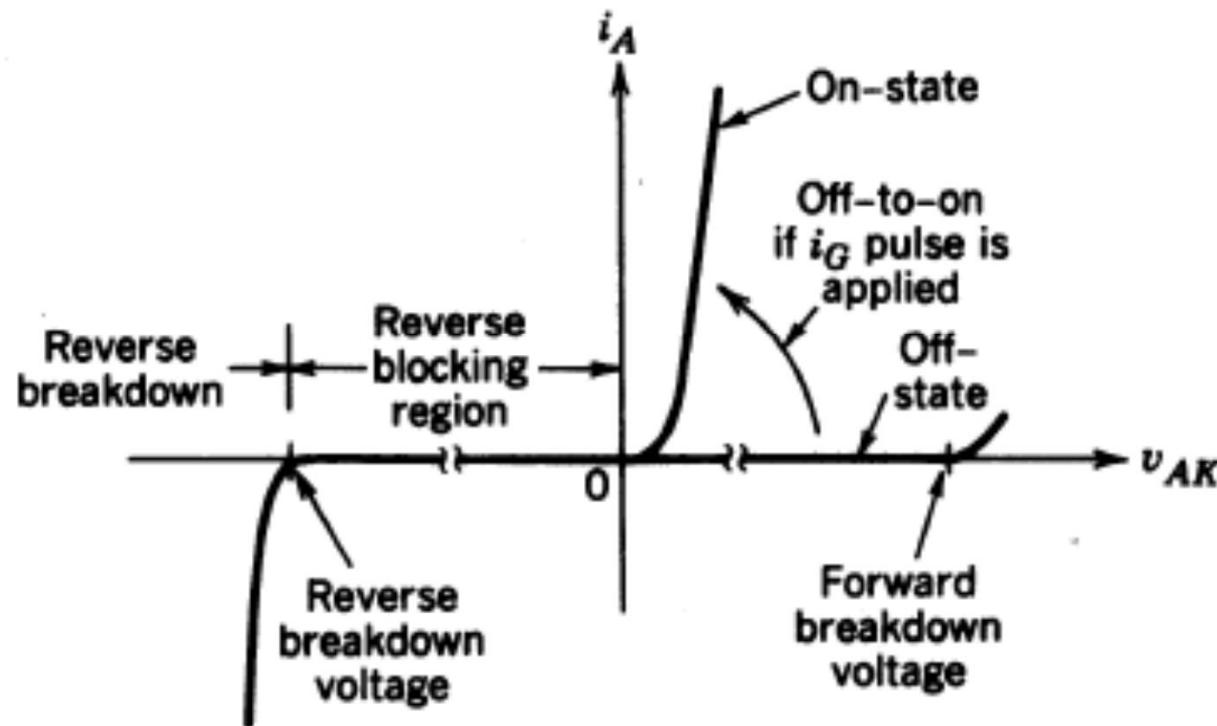
Thyristors

- Only possible to turn on
- Pulse on gate when forward blocking turns on thyristor
- Current reversal followed by reverse blocking turns off thyristor
- 3 modes:
 - Forward blocking
 - On-state
 - Reverse blocking

Thyristor circuit symbol.

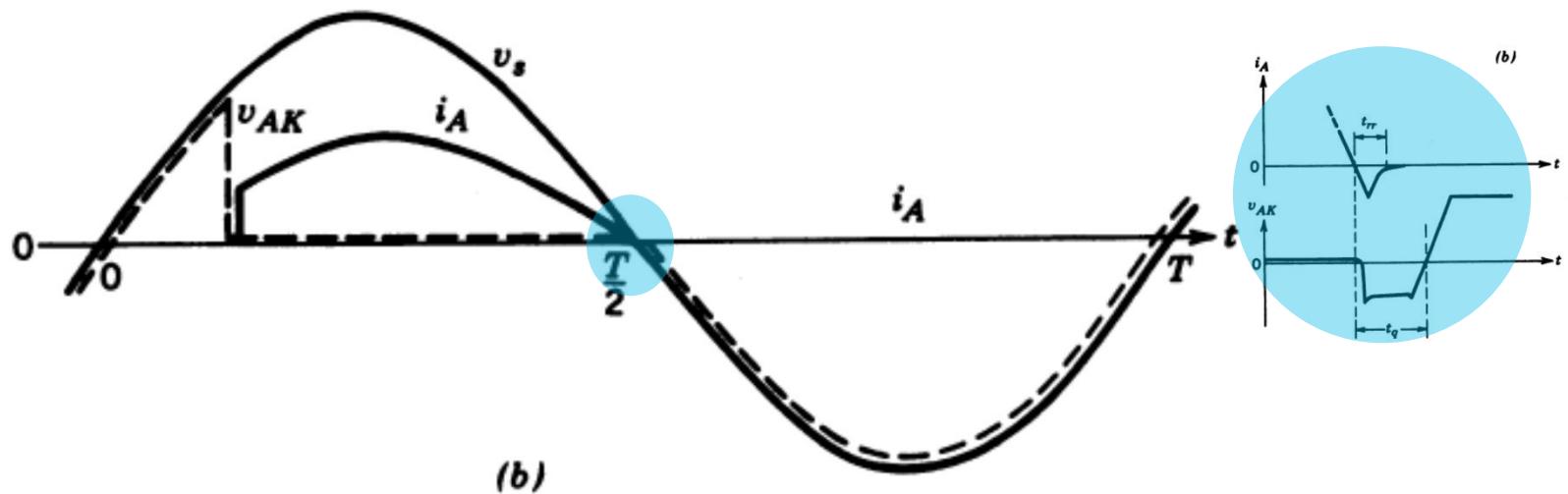
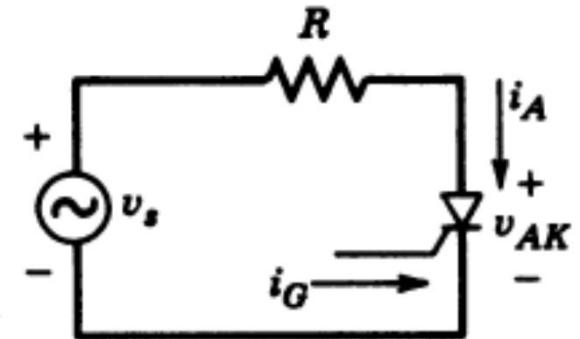


Actual thyristor characteristics



Thyristor, example circuit

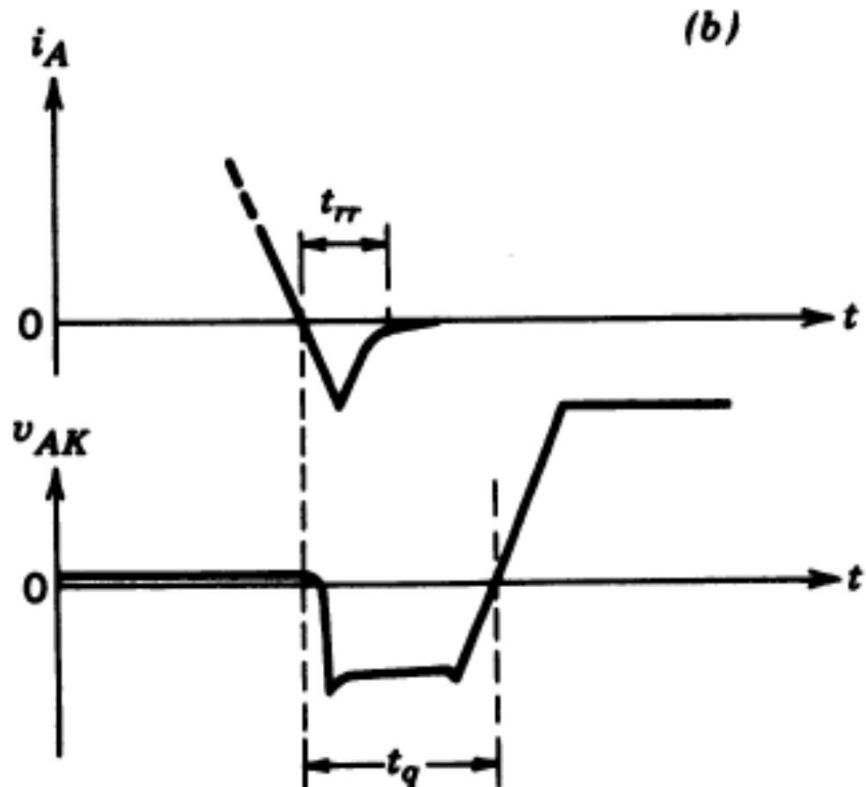
- Thyristor can be triggered in interval
 $0 < t < T/2$



Thyristor turn-off process

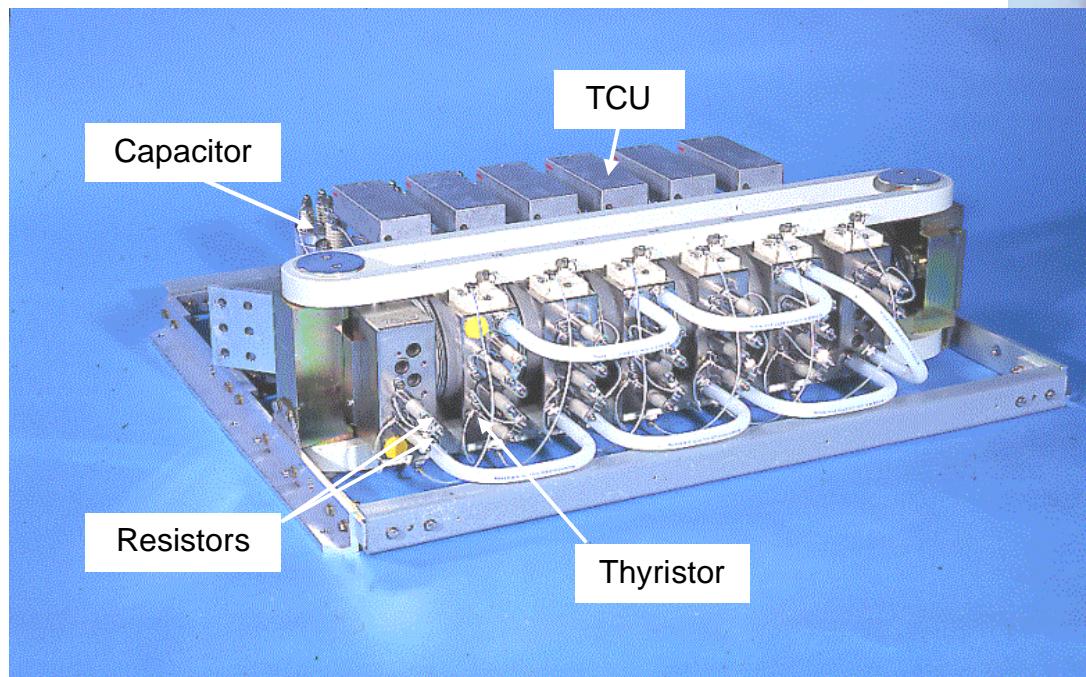
Succesful turn-off:

- Current reversal
 - reverse recovery as a diode
- Reverse blocking for $t \geq t_q$



Thyristor presspack

- Active part on a single silicon wafer.



ABB

Thyristor, junction structure

Two transistor equivalent circuit

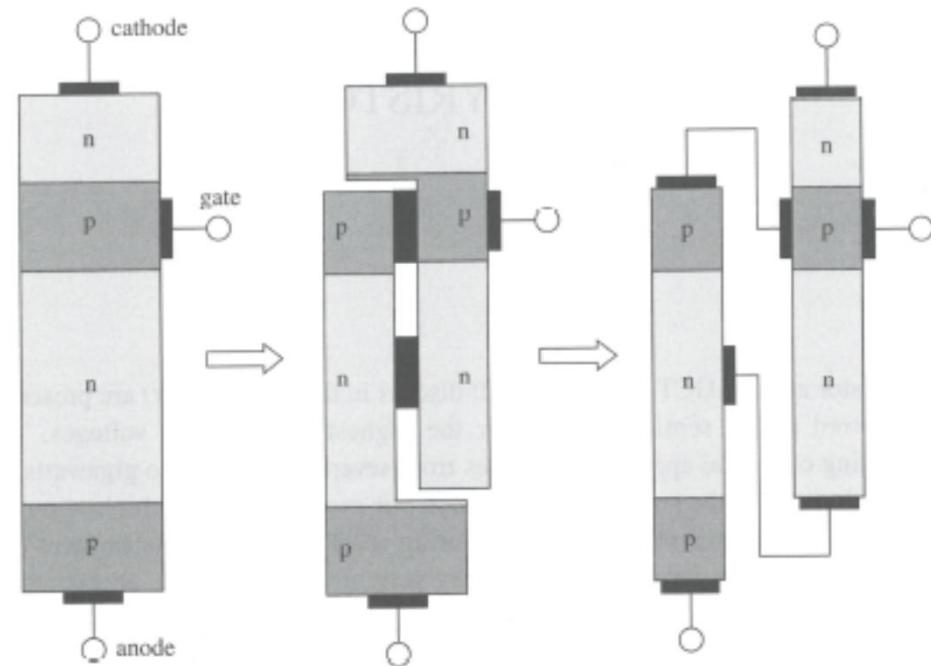
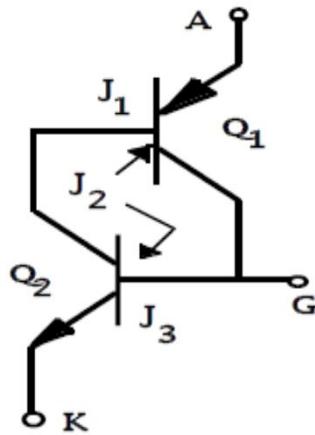


Fig. 5.1 Left: basic structure of the thyristor. Right: an equivalent model consisting of two bipolar transistors.

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Thyristor triggering to latched on-state

- $I_{C2} = \beta_2 I_G$
 - β : common emitter current gain
- $I_{B1} = I_{C2}$
- $I_{C1} = \beta_1 I_{B1}$
- $I_{B2} = I_{C1}$
- $I_{C1} = \beta_1 \beta_2 (I_G + I_{C1})$
- *Thyristor trigger at $\beta_1 \beta_2 \geq 1$*
- $\beta = \frac{\alpha}{1-\alpha}$ where α : common base current gain
- $\Rightarrow \alpha_1 + \alpha_2 \geq 1$

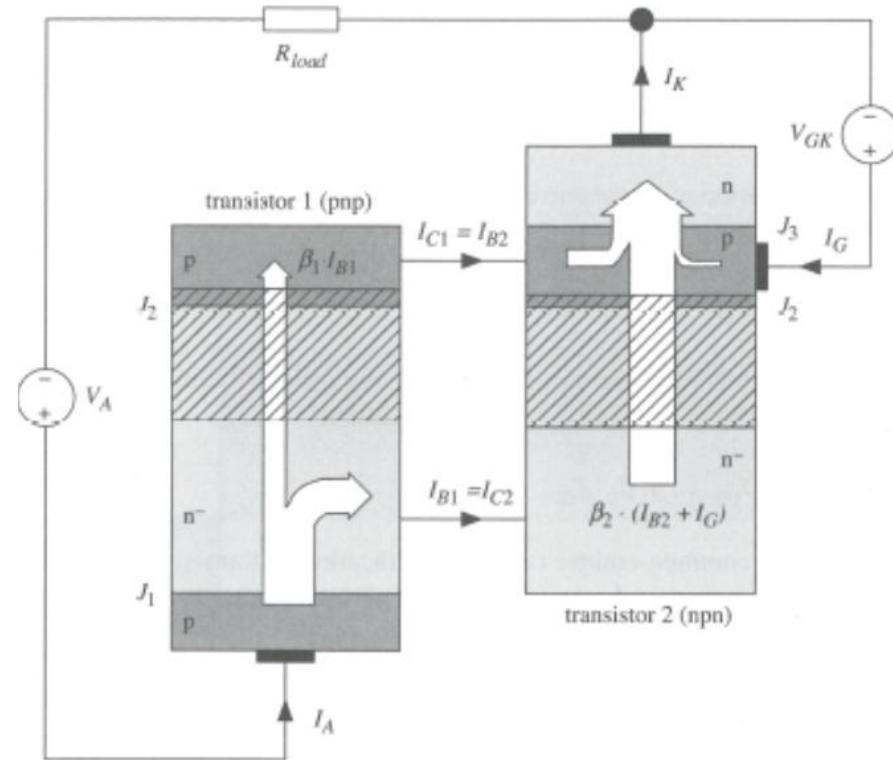
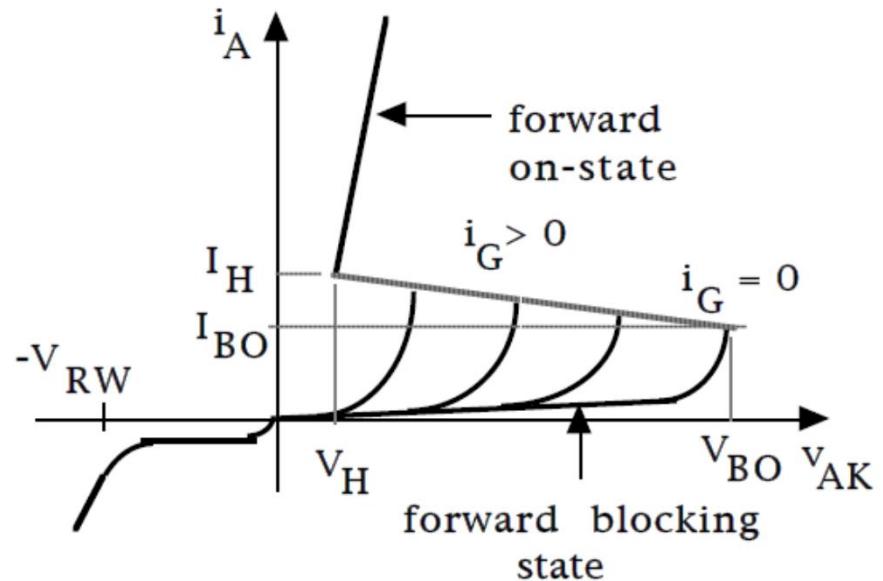


Fig. 5.2 Operation of the thyristor.

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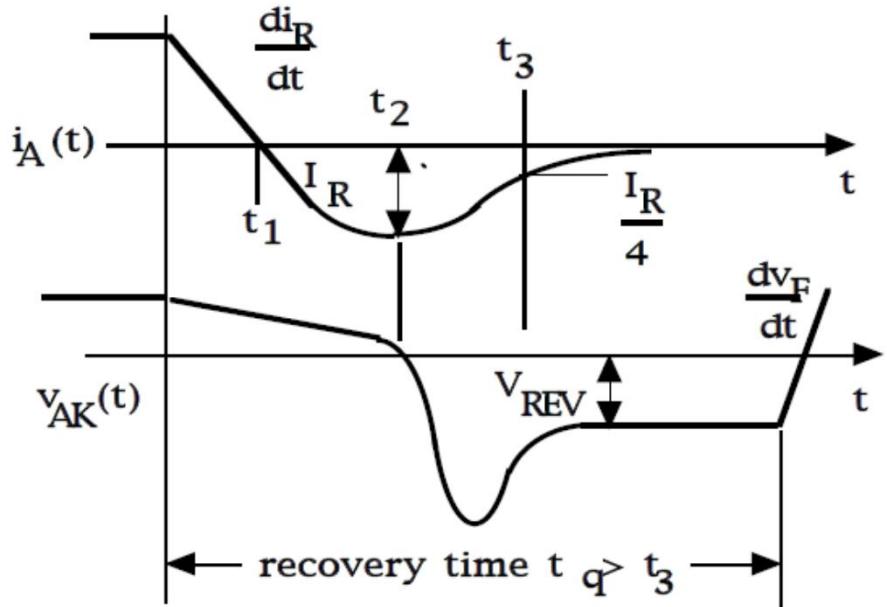
Thyristor, non-ideal characteristics

- I_H = Holding current
 V_H = holding voltage
- I_{BO} = Breakover current
 V_{BO} = Breakover voltage
- i_G can be a current pulse
- V_{RW} = Reverse working voltage
 - Thyristors found with $V_{RW} > 7\text{kV}$
- Forward voltage drop only a few volts even at $I_A > 2\text{kA}$



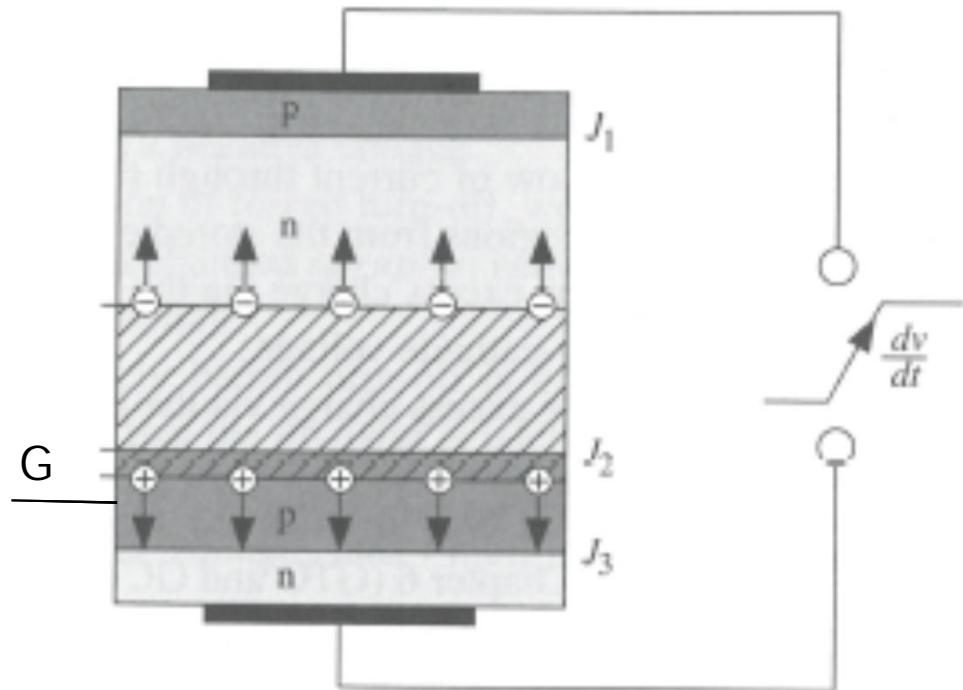
Thyristor turn-off timing

- Turn-off similar to diode
- Thyristor turn-off require negative V_{AK} longer than t_q (otherwise still on)
- dV_F/dt limit to keep thyristor off
(fast forward voltage increase may turn on thyristor!)



dV_A/dt triggering

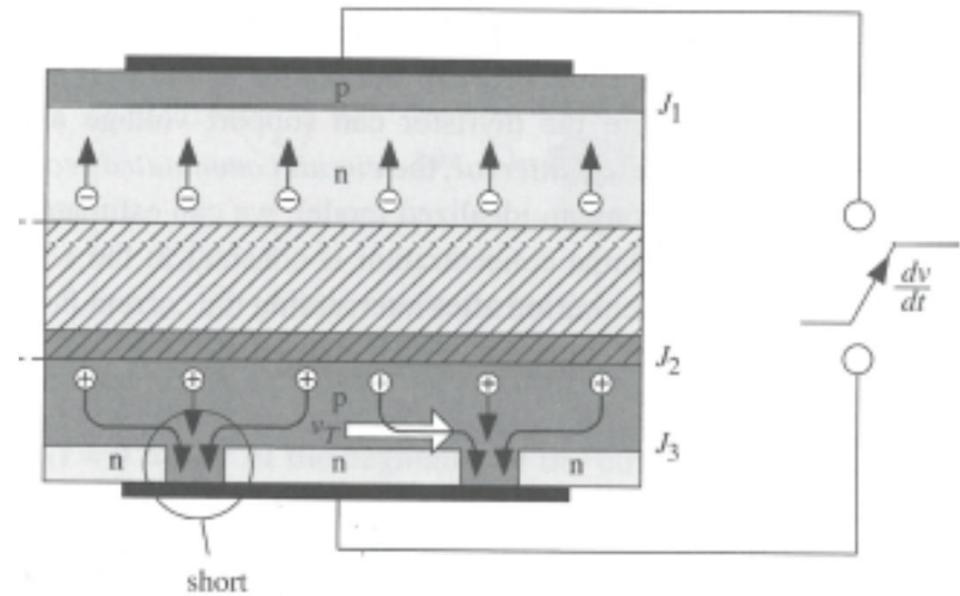
- Forward blocking
- Junction J2 is depleted and has a capacitance
- High dV_A/dt will charge C_{J2} .
- Charging current through pn-junction J3 may trigger the thyristor



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Improved dV_A/dt capability

- Emitter shorts
- Provide a current path bypassing the pn-junction J3
- On-state voltage drop increased related to



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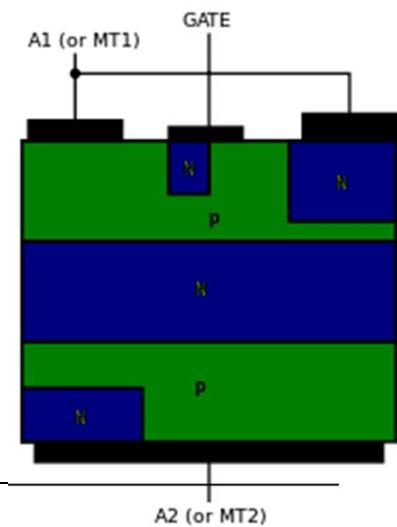
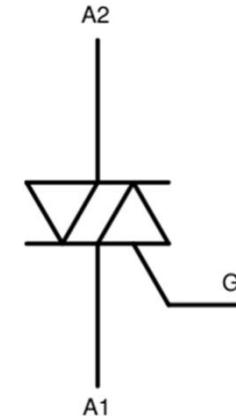
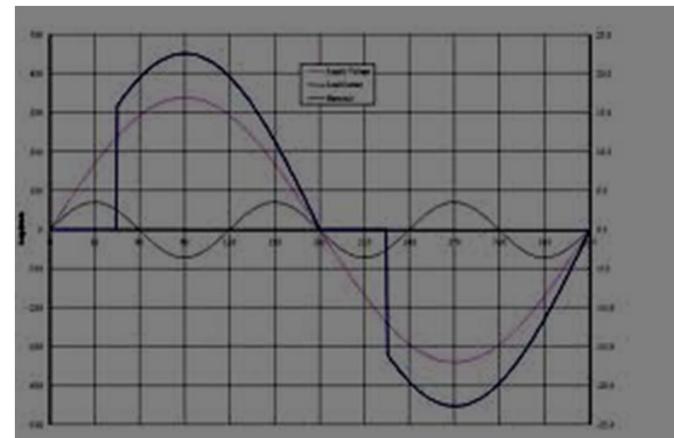
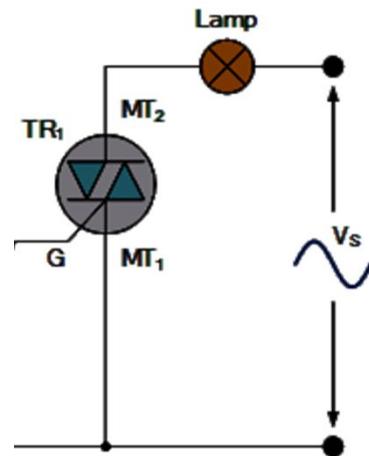
Thyristor types

- Phase-control
 - Used for rectifying line-frequency voltages and currents, low on-state voltage and large voltage and current range
 - $> 4 \text{ kA}$, $> 7 \text{ kV}$, 1.5 - 3 V on-state voltage
- Inverter-grade
 - Small turn-off time ($1 \text{ us} < t_{qf} < 100 \text{ us}$) and low on-state voltages
- Light-triggered
 - Trigger by light pulse instead of current
 - Used in high-voltage applications, where series connected thyristors used to support high voltages
 - $\sim 5 \text{ mW}$ light pulse to trigger

Datasheet

Support current in both directions: Triac

- Function as antiparallel thyristor
- Enable triggering on both positive and negative part of the cycle



Lecture 4

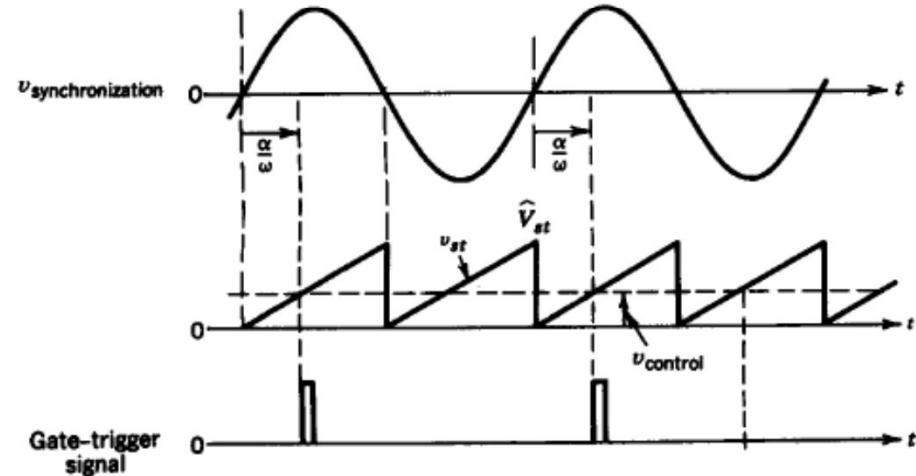
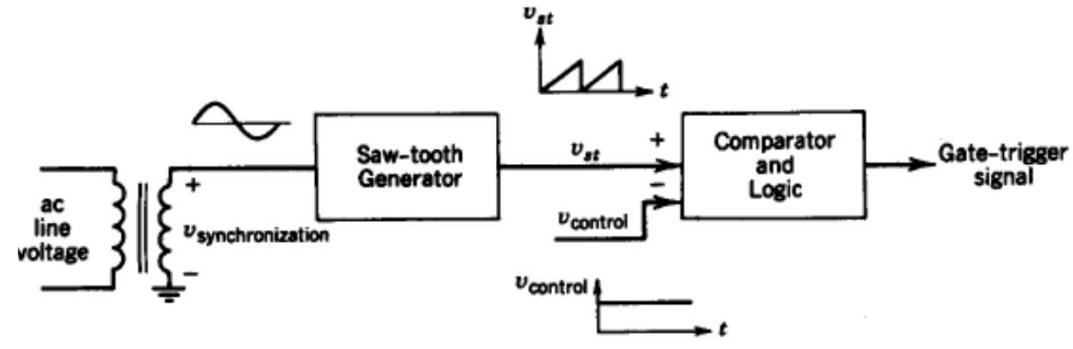
Thyristor operation

- Gate control
- Single phase
- Three phase
- Rectifier vs inverter mode

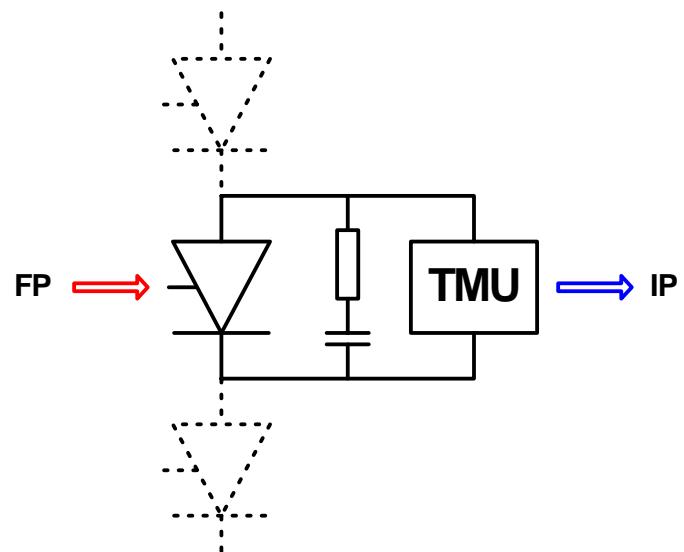
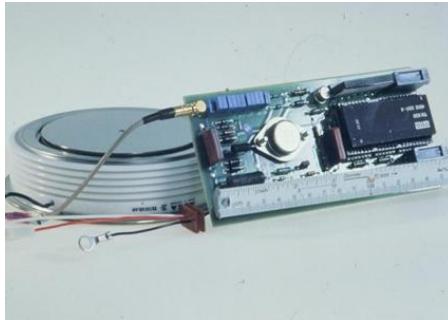
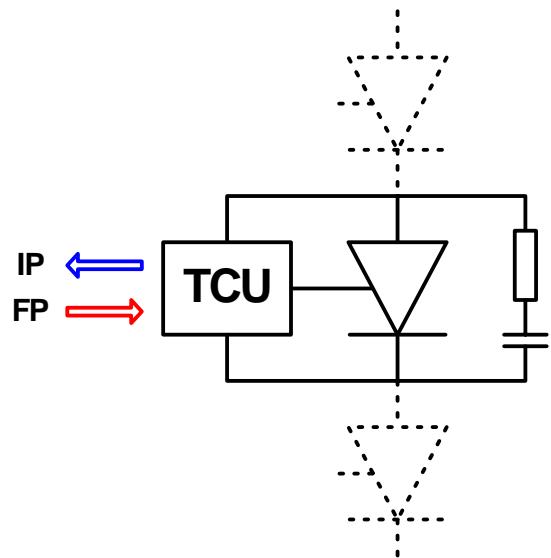
How to control gate

- IC circuits available

$$\alpha = 180 \frac{v_{control}}{V_{st}}$$



Thyristor triggering in HVDC applications



FP = Firing pulse

IP = Indicating pulse

Electrically triggered thyristor (ETT)

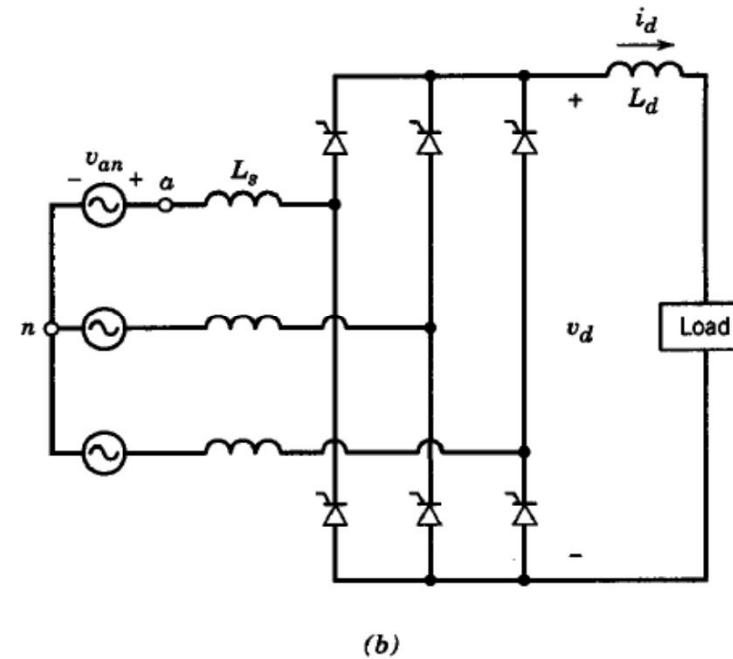
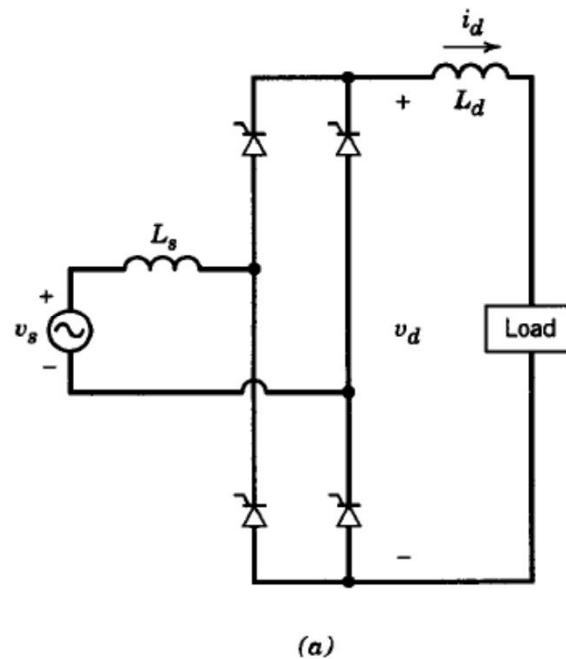
- The ETT is triggered by the thyristor control unit (TCU).
- The TCU is energized by the main circuit, and triggering is initiated by an optical pulse
- The TCU protects and monitors the ETT

Light-triggered thyristor (LTT)

- The LTT is triggered directly by an optical pulse
- The LTT is self-protected against overvoltage
- Separate recovery protection is provided
- The TMU monitors the LTT

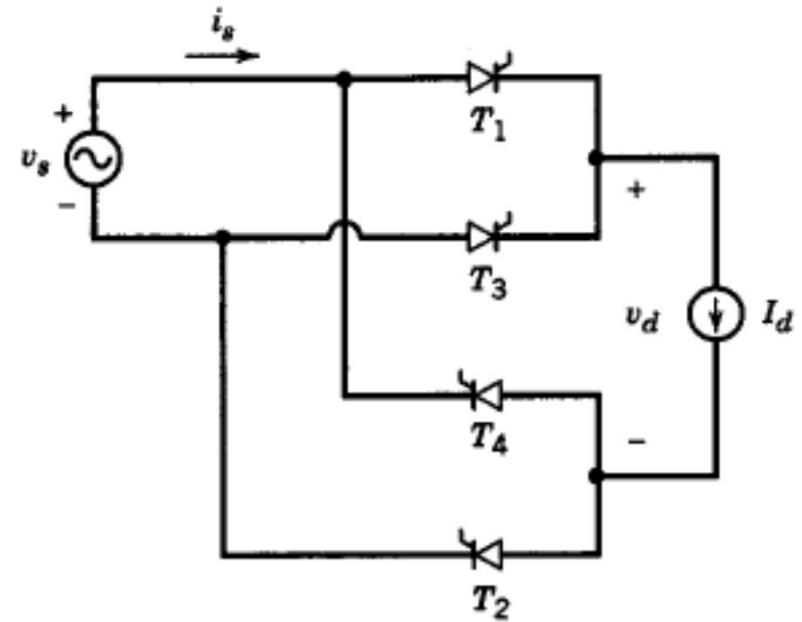
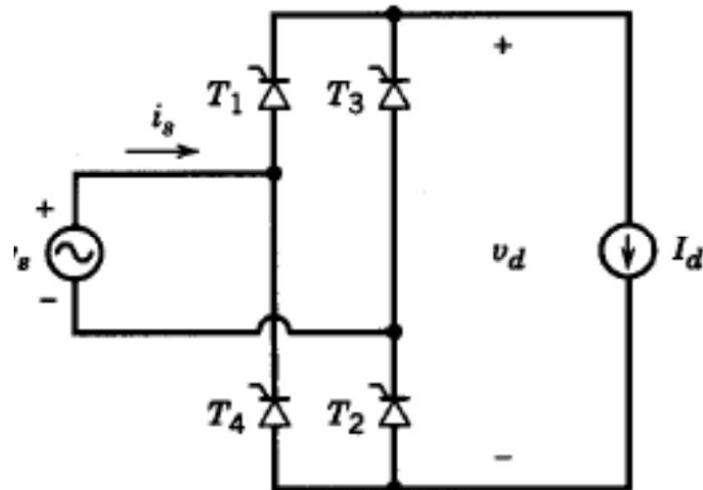
Full bridge thyristor converters

- Includes source inductance L_s and load inductance L_d
- Source inductance



Single-phase thyristor converter

- Either thyristor T1 and T2, or T3 and T4 conducting



Single-phase thyristor converter waveforms

- I_d constant \Rightarrow thyristor does not turn off unless other thyristor turns on (current commutation)
- V_d and P controlled by α

$$V_{d\alpha} = \frac{1}{\pi} \int_{\alpha}^{\pi+\alpha} \sqrt{2}V_s \sin \omega t d(\omega t) =$$

$$\frac{2\sqrt{2}}{\pi} V_s \cos \alpha = 0.9V_s \cos \alpha$$

$$P = I_d \left(\frac{1}{T} \int_0^T v_d dt \right) = I_d V_d = 0.9V_s I_d \cos \alpha$$

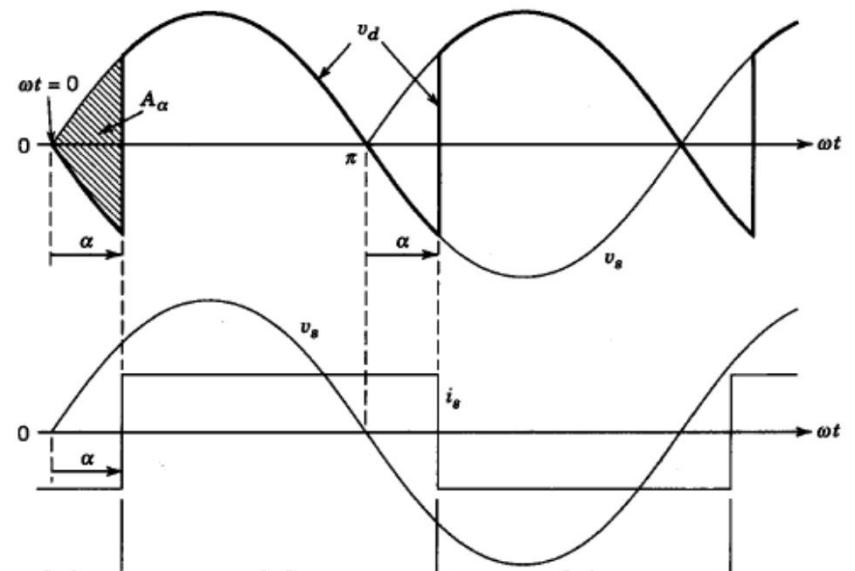
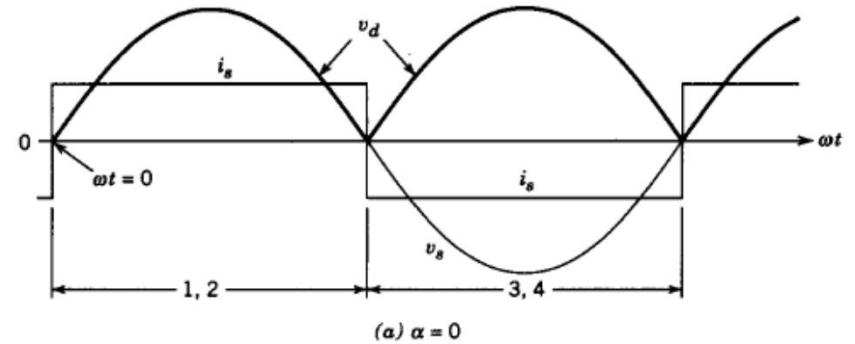
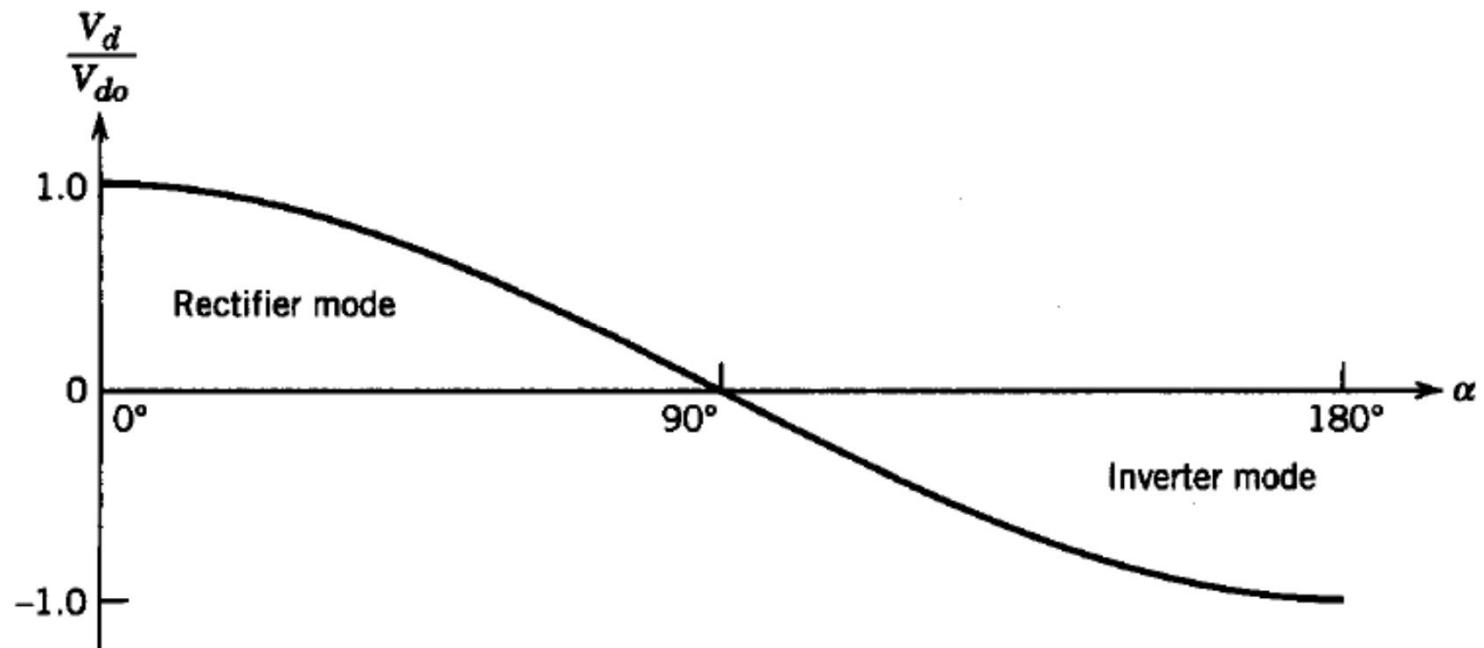


Figure 6-6 Waveforms in the converter of Fig. 6-5.

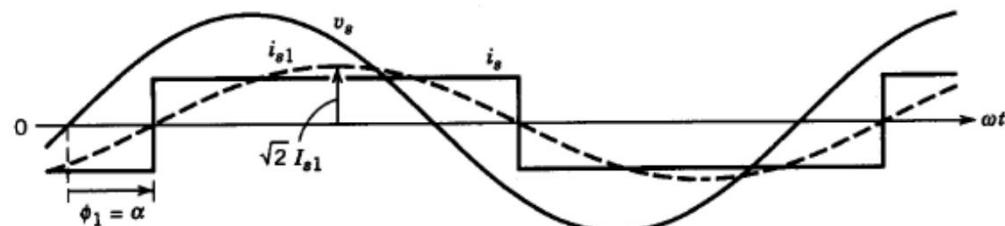
DC voltage level

- Power from DC to AC side when $\alpha > 90$ degrees

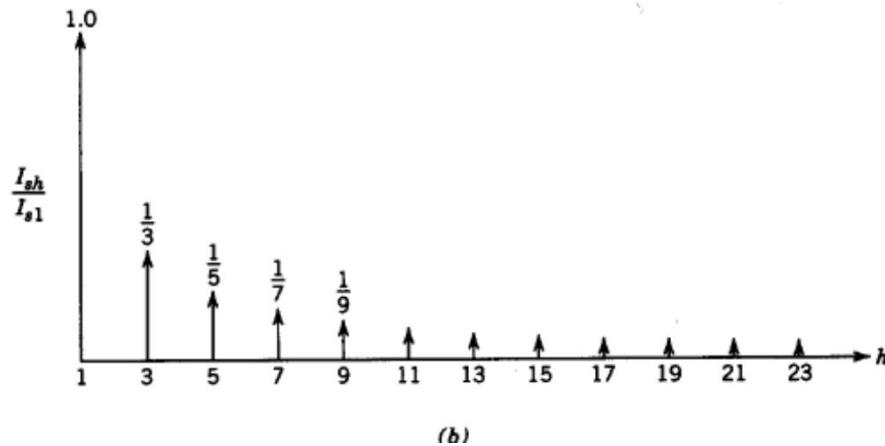


Line current properties

$$\begin{aligned}I_{s1} &= 0.9I_d \\I_s &= I_d \text{ (rms)} \\THD &= 48.3\%\end{aligned}$$



(a)



(b)

Power, power factor, reactive power

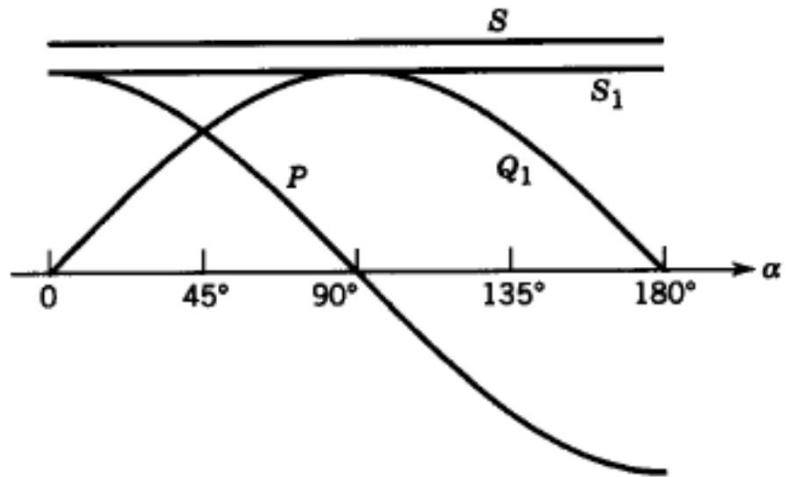
$$DPF = \cos\Phi_1 = \cos\alpha$$

$$PF = \frac{I_{s1}}{I_s} DPF = 0.9\cos\alpha$$

$$P = V_s I_{s1} \cos\Phi_1 = 0.9V_s I_d \cos\alpha$$

$$Q_1 = V_s I_s \sin\Phi_1 = 0.9V_s I_d \sin\alpha$$

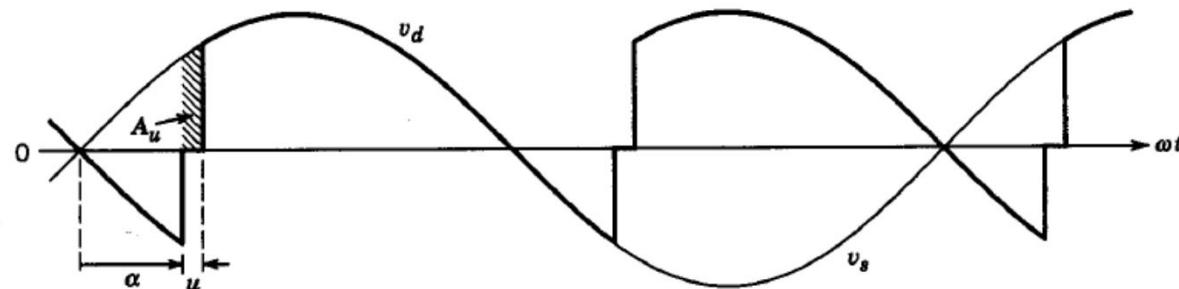
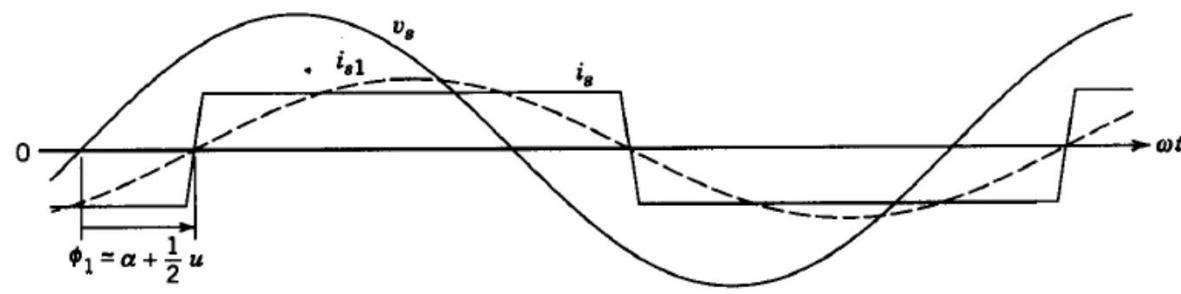
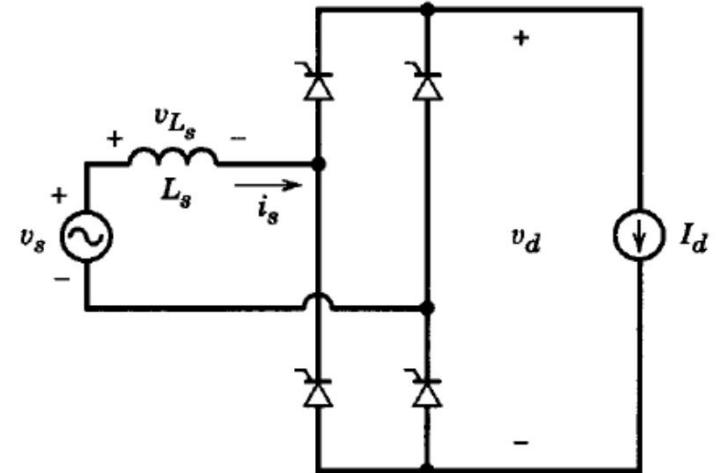
$$S_1 = V_s I_{s1}$$



L_s effect

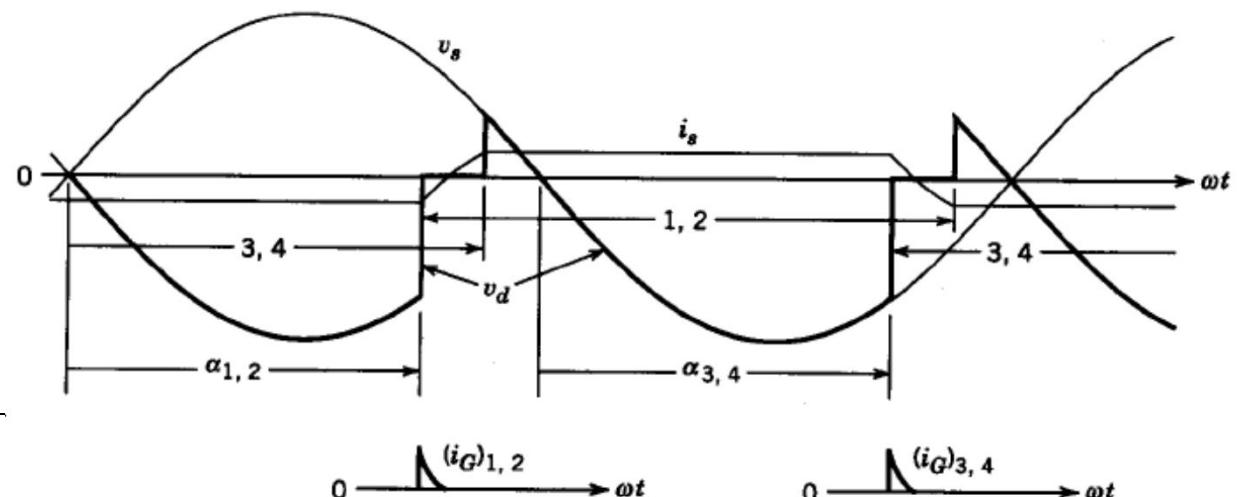
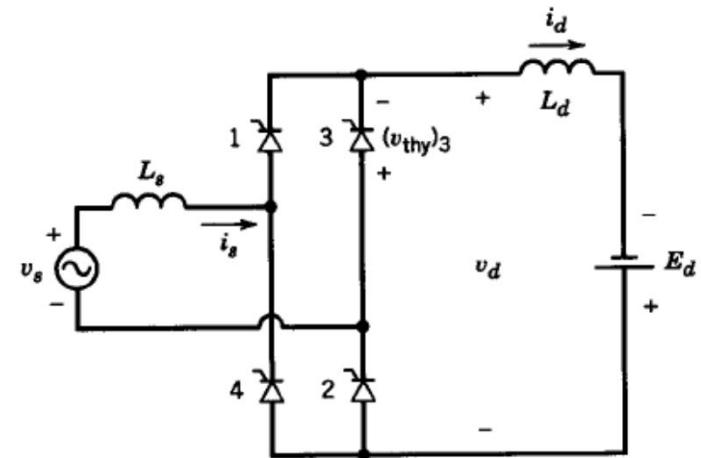
$$A_u = 2\omega L_s I_d \cos(\alpha + u) = \cos\alpha - \frac{2\omega L_s I_d}{\sqrt{2}V_s}$$

$$V_d = 0.9V_s \cos\alpha - \frac{2}{\pi} \omega L_s I_d$$



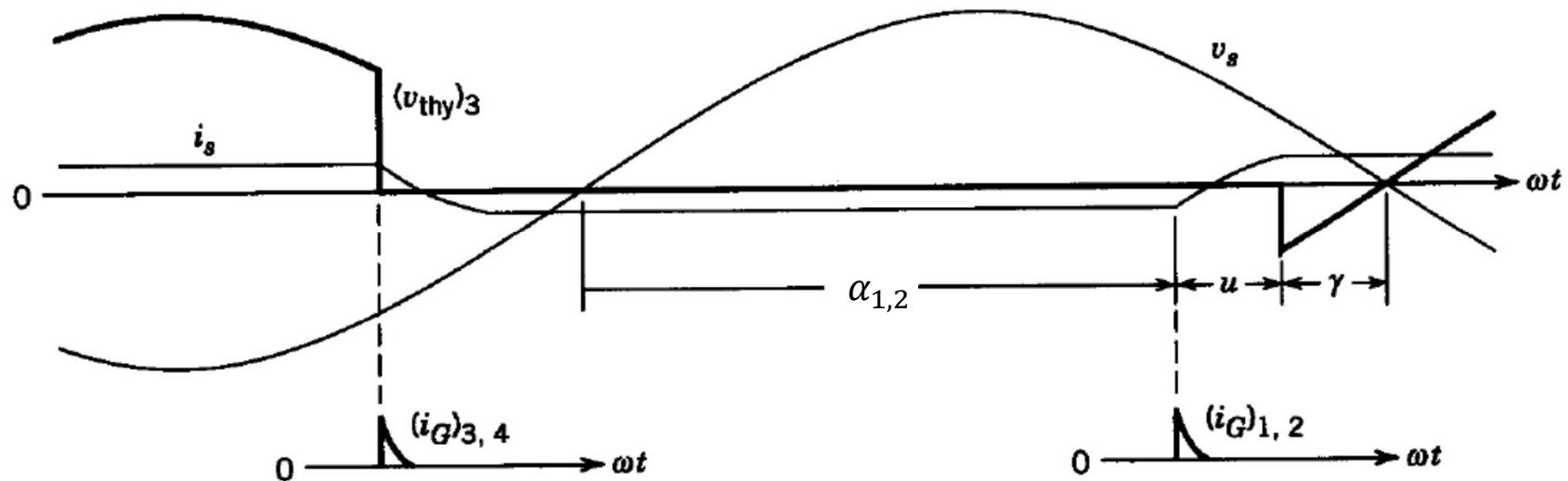
Inverter mode

- Negative dc-side voltage, v_d , E_d
- Always positive current. Thyristor conducts in one direction only
- $P < 0$: $(v_d < 0)(i_d > 0)$
- Power flows from DC to AC side
- V_s controls switching of current between thyristors



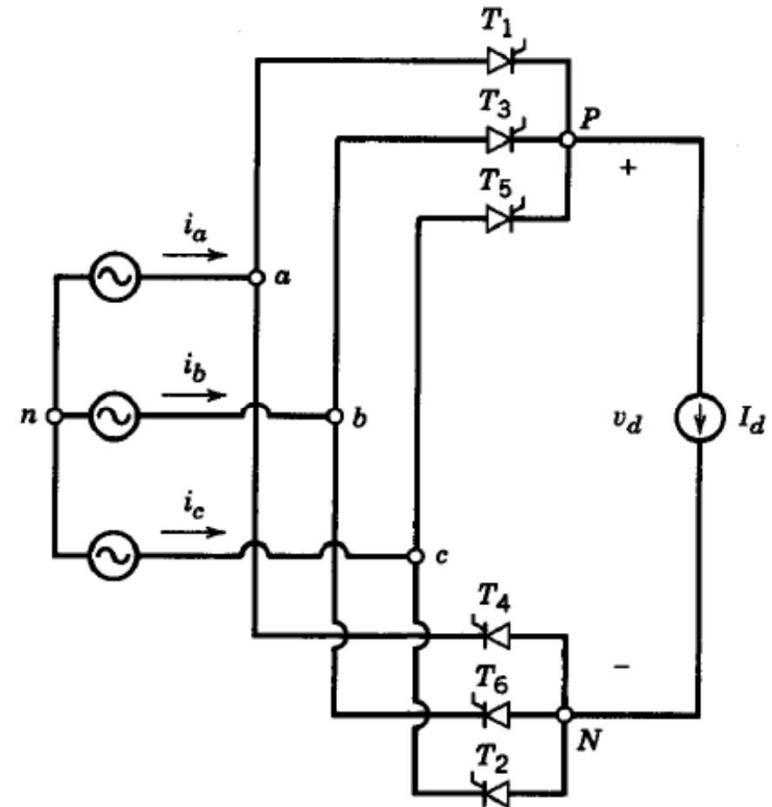
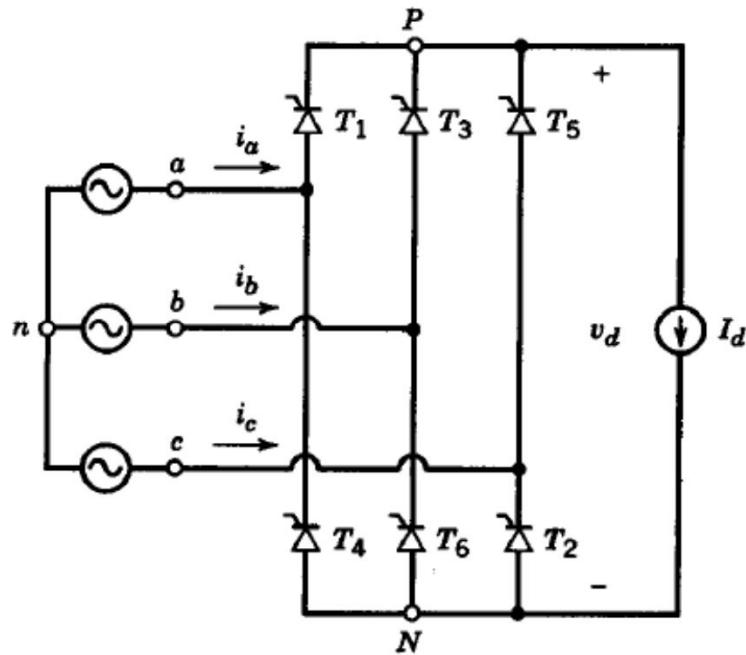
Inverter thyristor voltage

- Extinction angle $\gamma = 180 - (\alpha + u)$
- Thyristor require $t_\gamma = \gamma/\omega > t_q$ (turn off time)
- Failing requirement leads to retriggering of the thyristor too early (commutation failure)
=> large currents (all thyristors conduct for long time)!

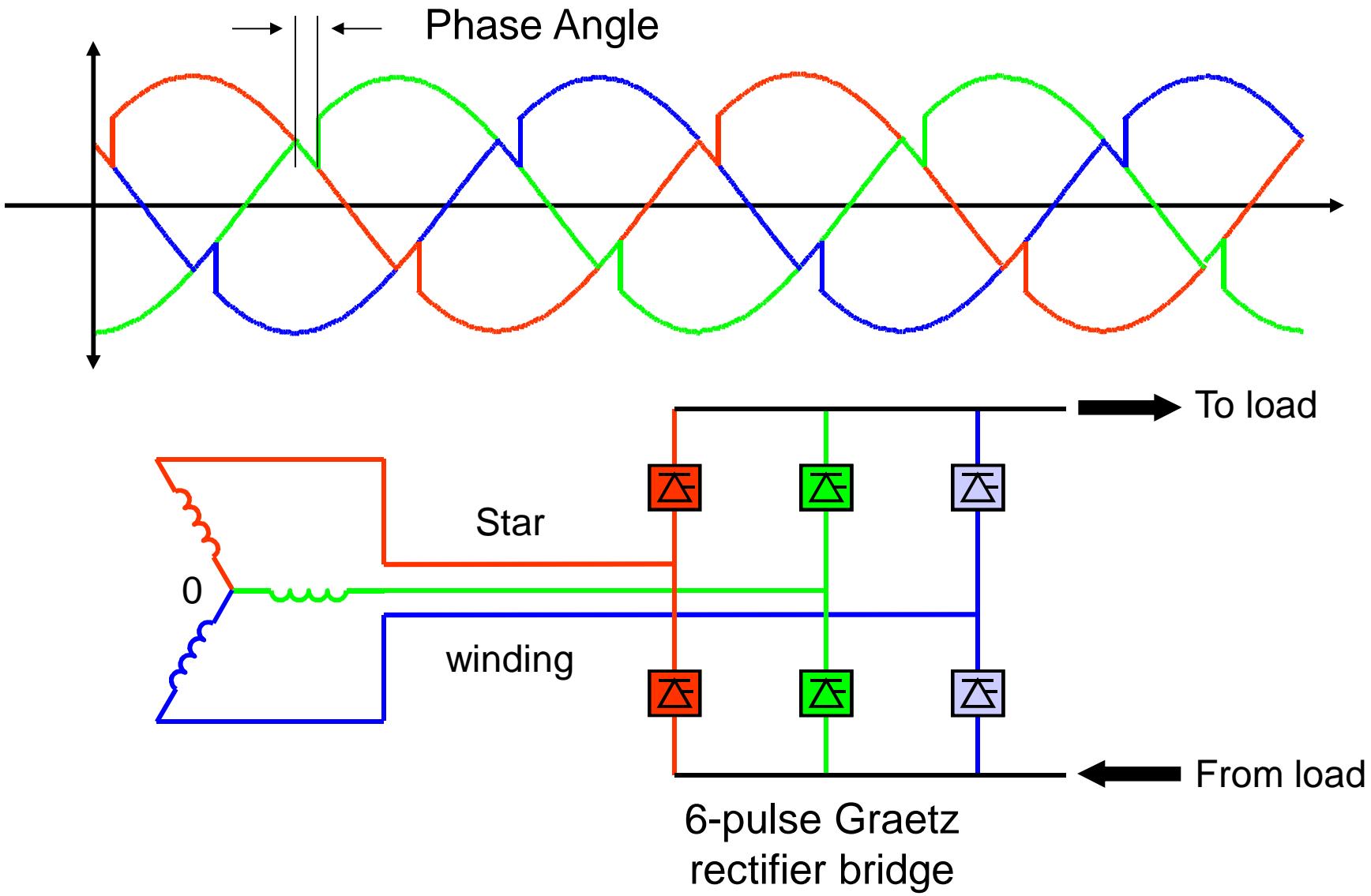


Three-phase thyristor converter

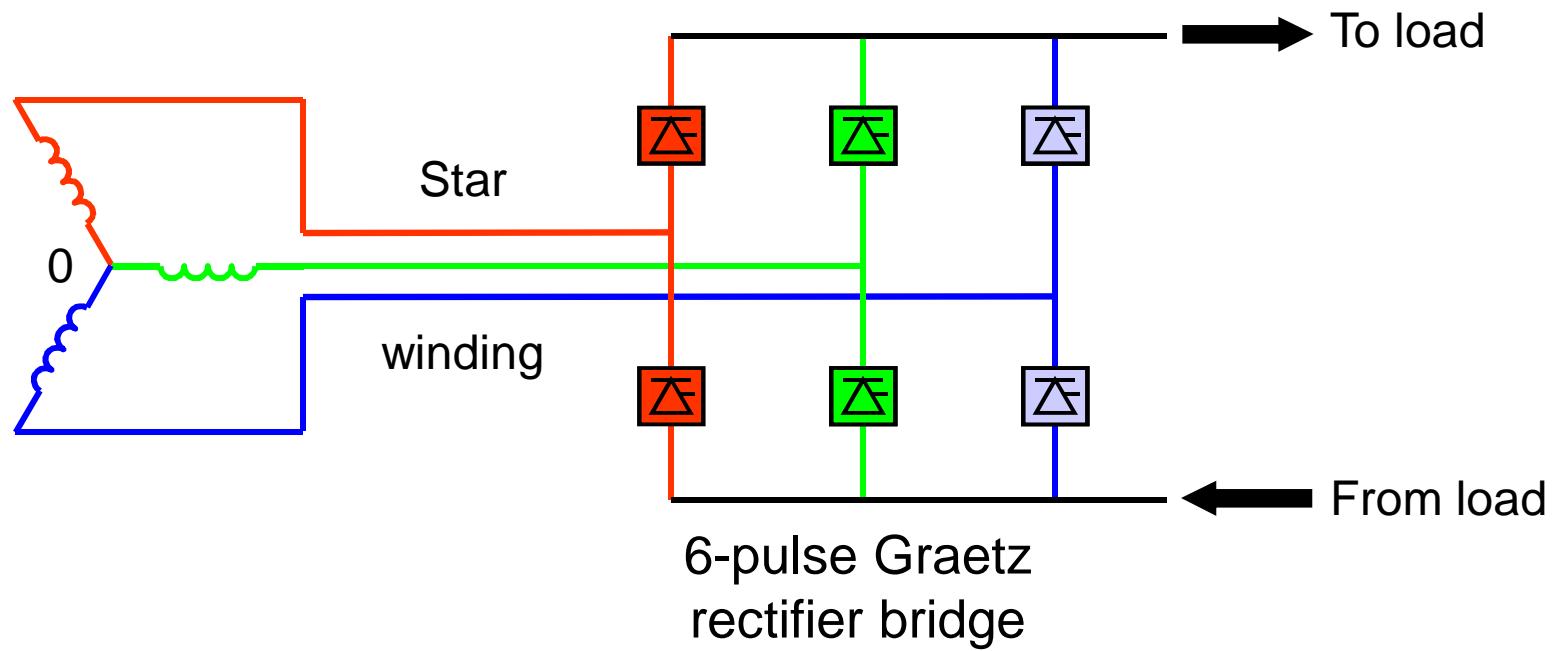
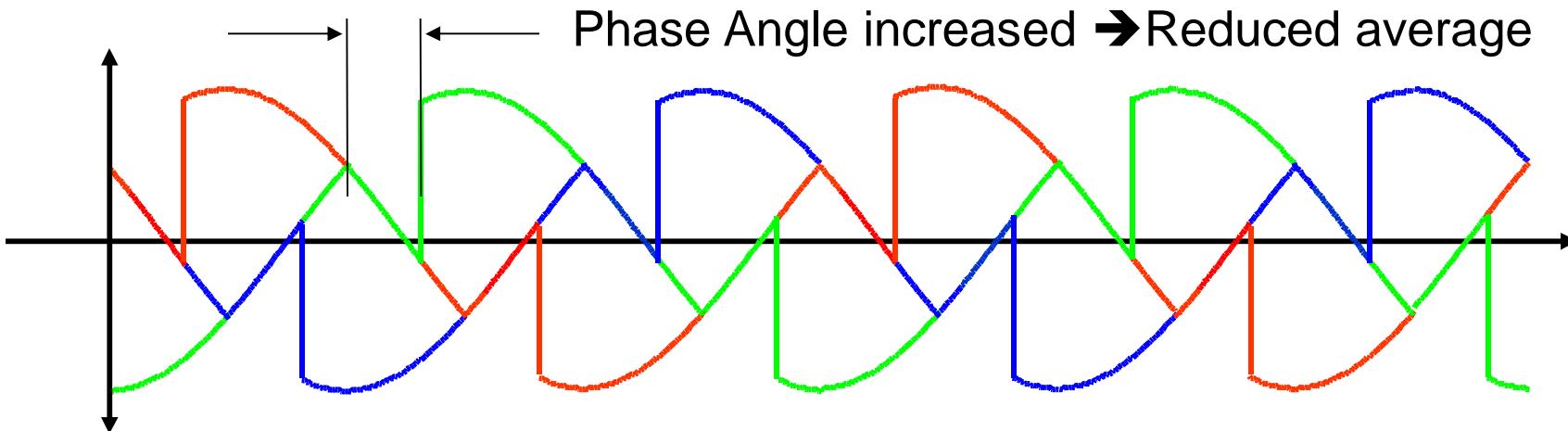
- One thyristor active in top group and one in bottom group



Thyristor rectifier operation



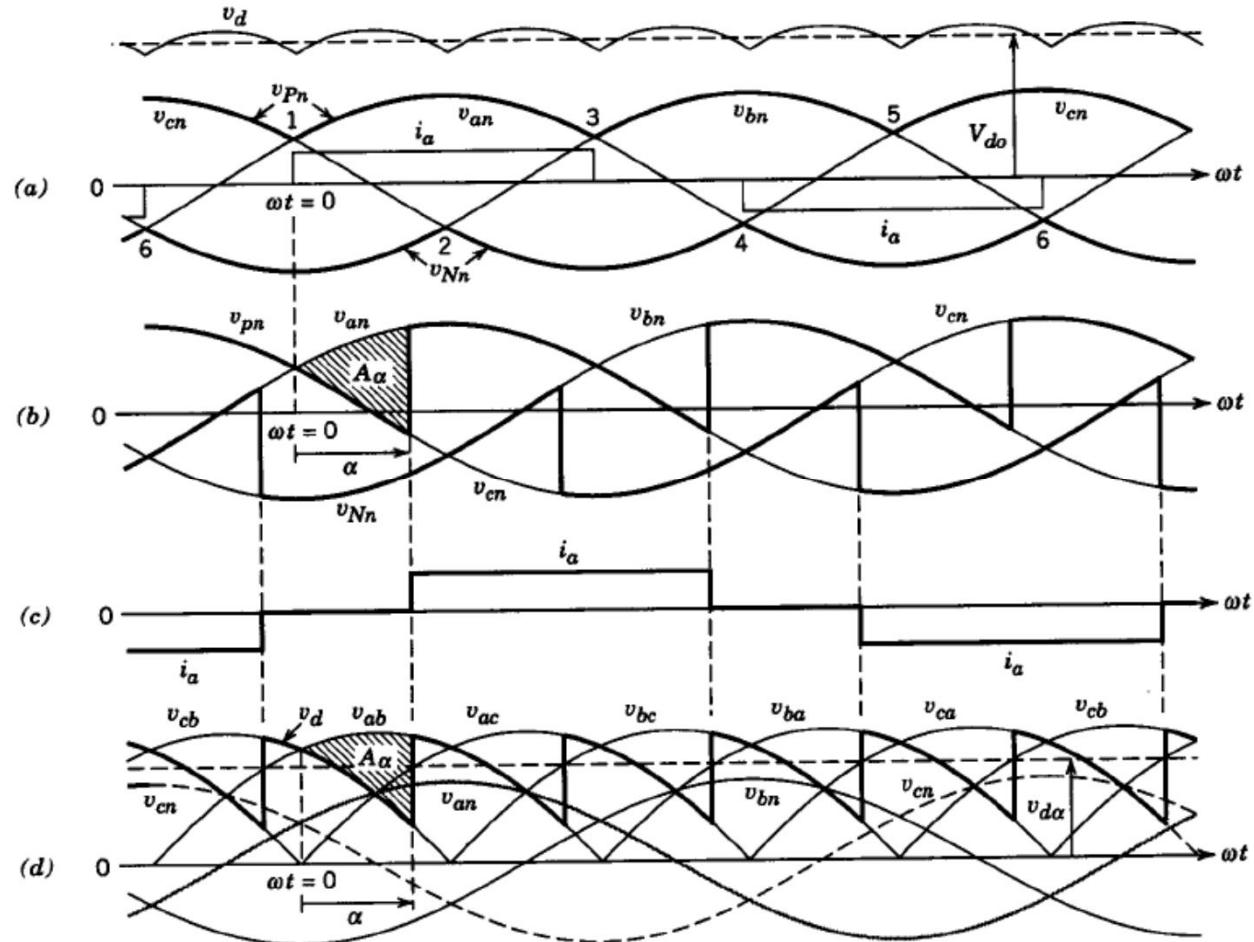
Thyristor rectifier operation



Converter waveforms

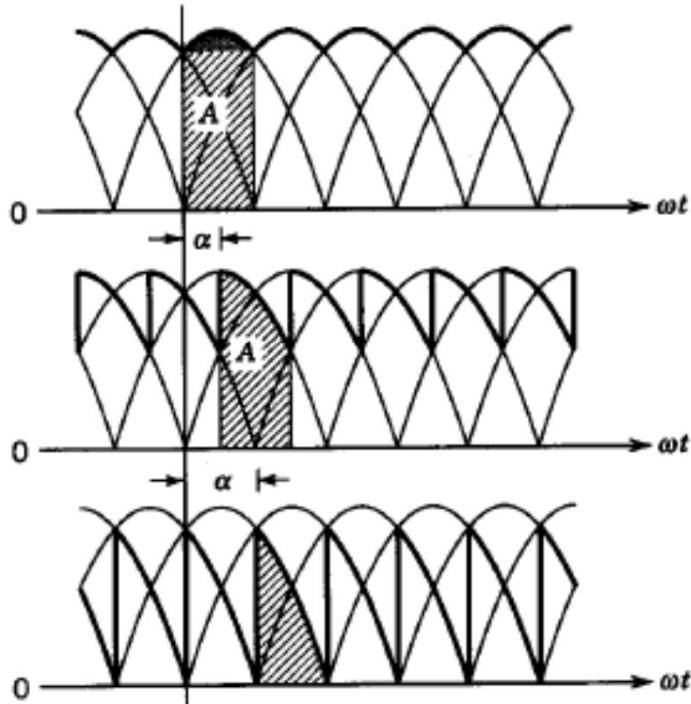
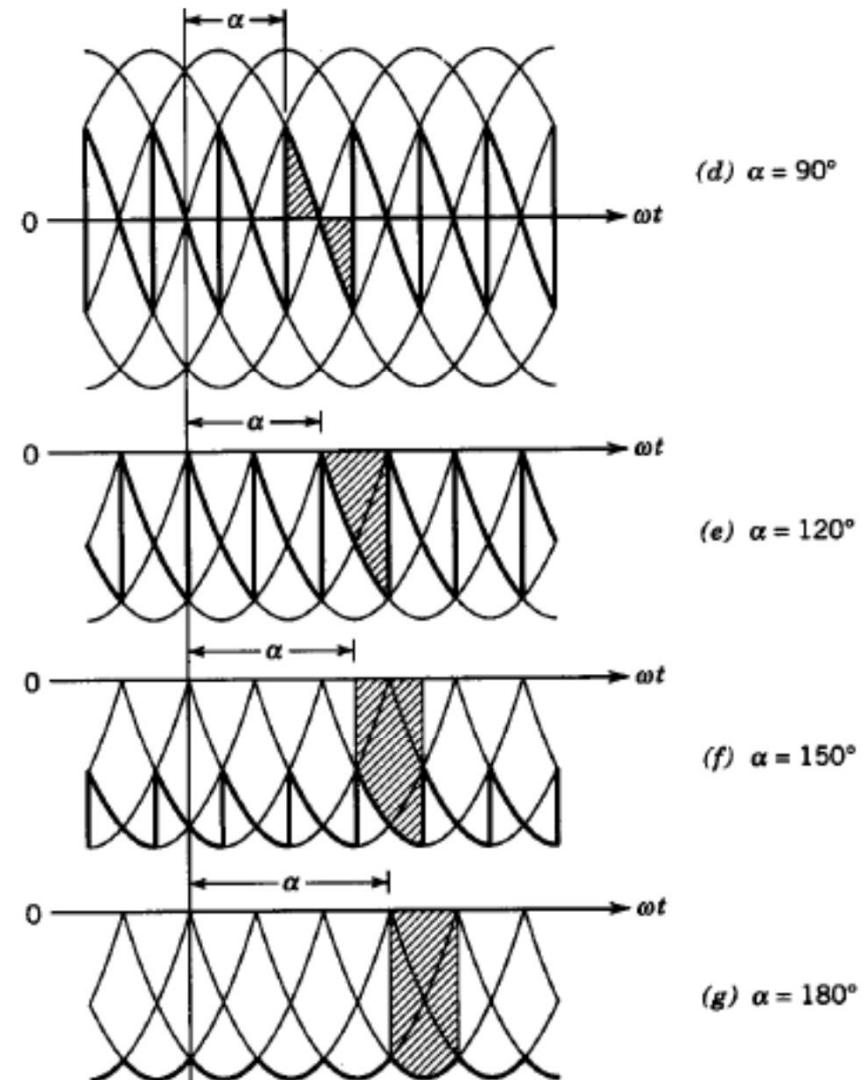
$$V_{d\alpha} = \frac{3\sqrt{2}}{\pi} V_{LL} \cos \alpha$$

$$V_{d\alpha} = 1.35 V_{LL} \cos \alpha$$

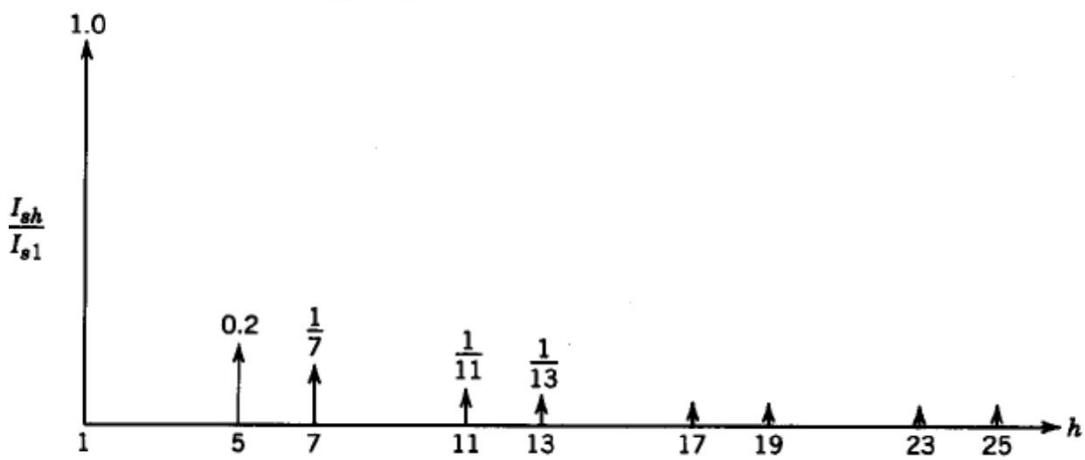
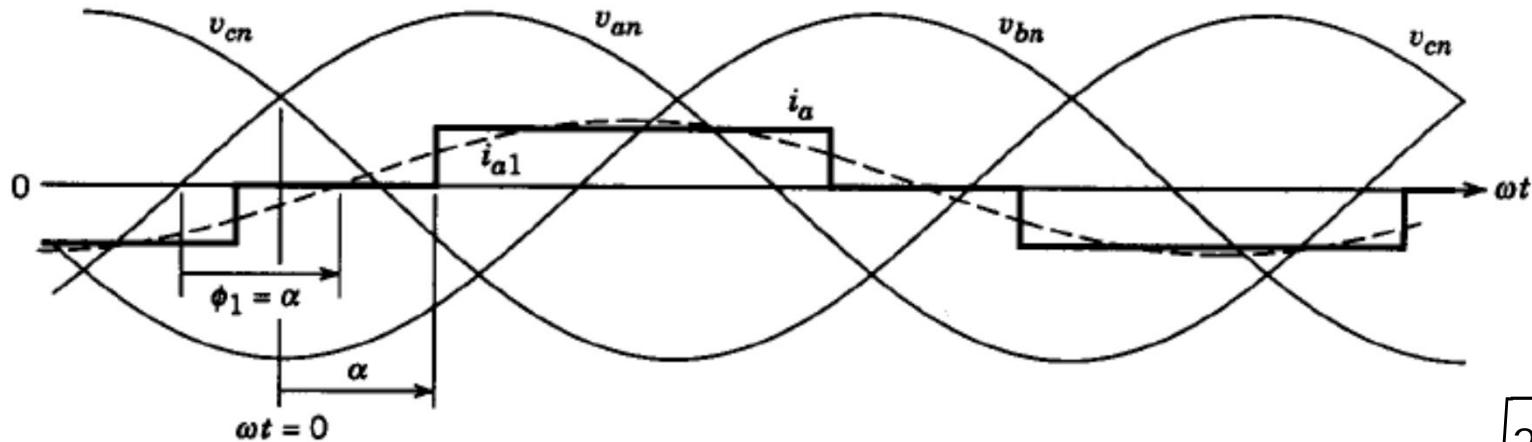


DC side voltage

- AC ripple frequency six times the line frequency

(a) $\alpha = 0$ (b) $\alpha = 30^\circ$ (c) $\alpha = 60^\circ$ (d) $\alpha = 90^\circ$ (e) $\alpha = 120^\circ$ (f) $\alpha = 150^\circ$ (g) $\alpha = 180^\circ$

Input line current



$$RMS\ current: I_S = \sqrt{\frac{2}{3}} \cdot I_d$$

$$I_{s1} = \frac{1}{\pi} \sqrt{6} I_d = 0.78 I_d$$

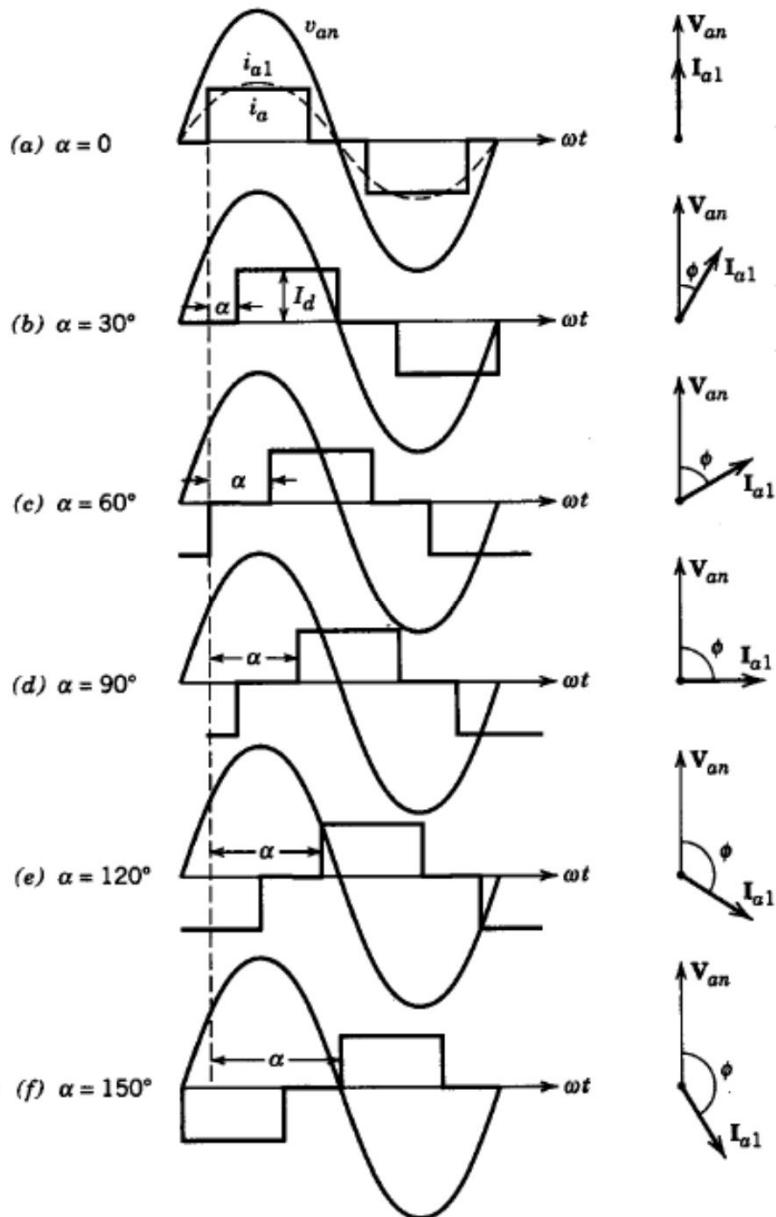
$$THD = \frac{\sqrt{\sum_{h=5,7,11,13,\dots} (I_{sh}^2)}}{I_{s1}} = 31\%$$

Line current vs alpha

- Current phase shift equal to α

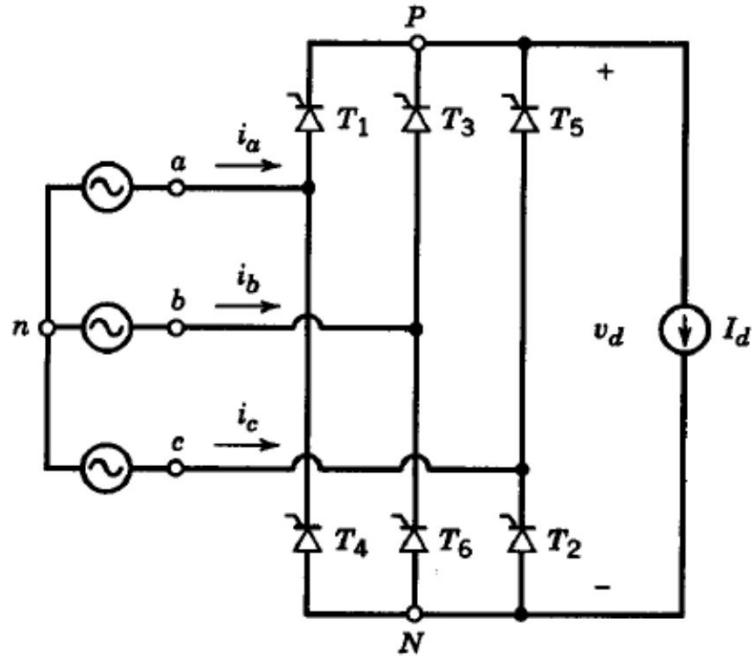
$$DPF = \cos\Phi_1 = \cos\alpha$$

$$PF = \frac{I_{S1}}{I_S} DPF = \frac{3}{\pi} \cos\alpha$$

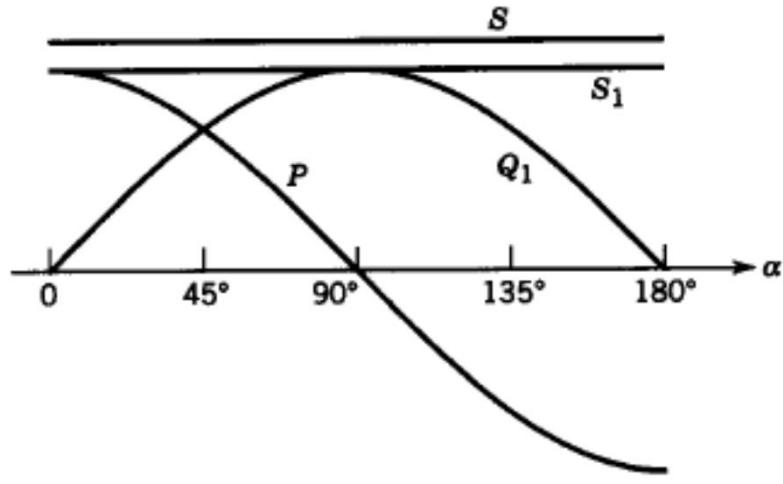


Exercise 4-100

- In the ideal three-phase thyristor rectifier circuit, the firing angle $\alpha=30$ deg
 - a) Construct the thyristor T_1 voltage and current
 - b) Construct the wave form of the dc-output voltage
 - c) Calculate the average dc-output voltage for $V_{LL}=400V$



Active and reactive power vs alpha

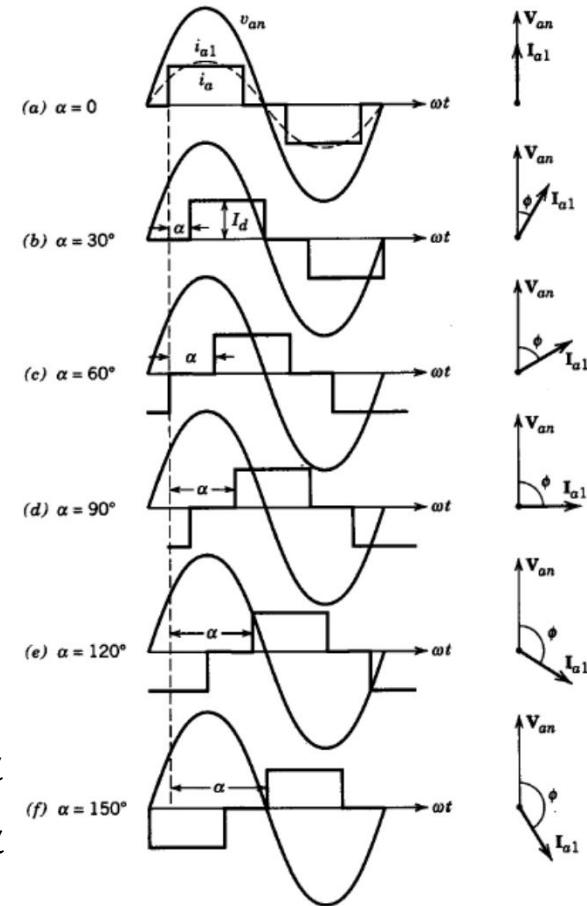


$$DPF = \cos\Phi_1 = \cos\alpha$$

$$PF = \frac{I_{s1}}{I_s} DPF = \frac{3}{\pi} \cos\alpha$$

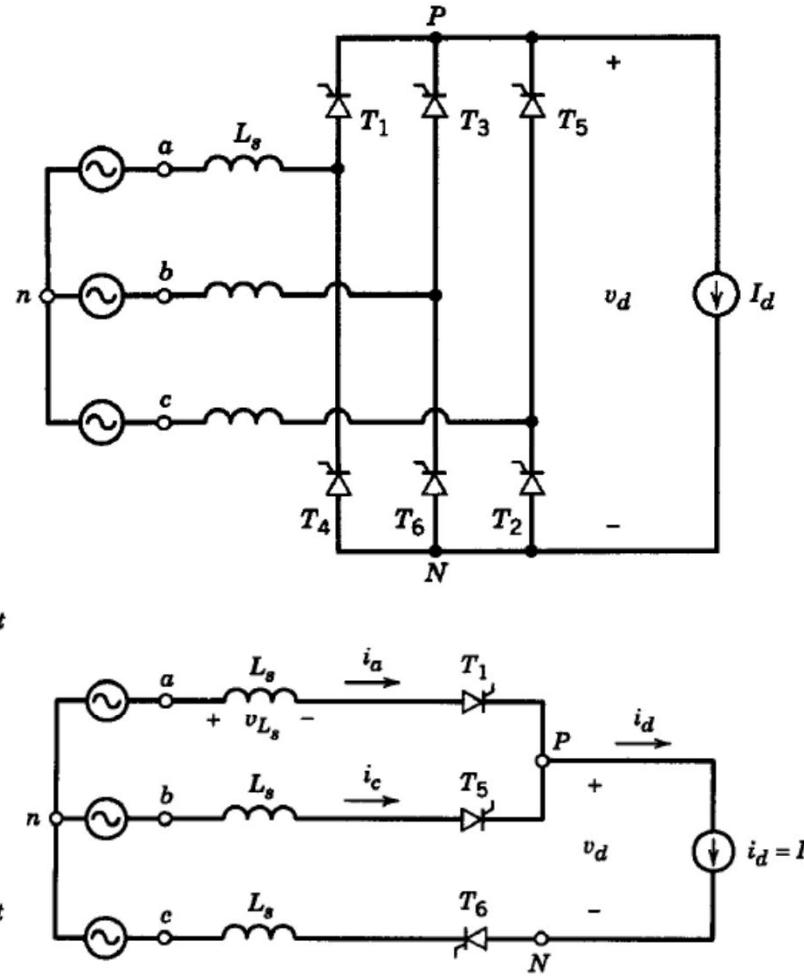
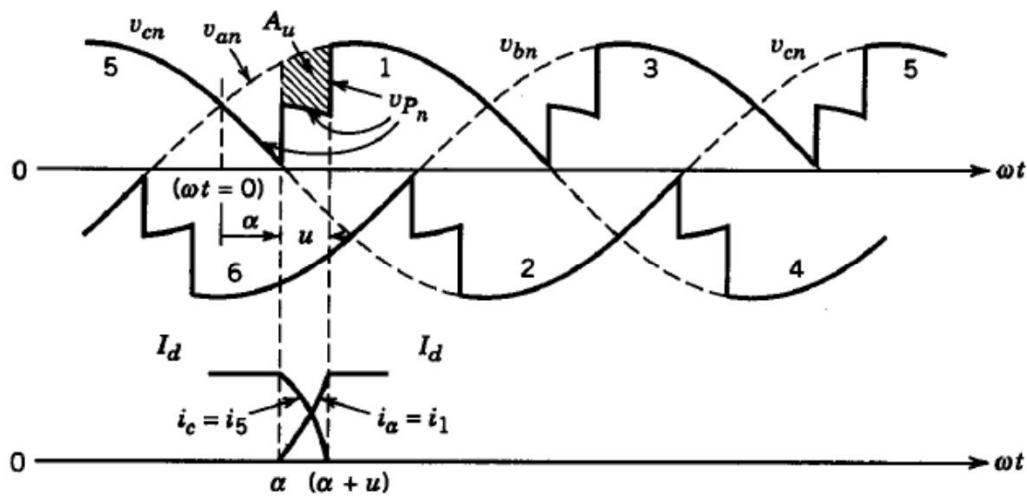
$$P = \sqrt{3}V_{LL}I_{s1}\cos\Phi_1 = \sqrt{3}V_{LL}0.78I_d\cos\alpha = 1.35V_{LL}I_d\cos\alpha$$

$$Q_1 = \sqrt{3}V_{LL}I_{s1}\sin\Phi_1 = \sqrt{3}V_{LL}0.78I_d\sin\alpha = 1.35V_{LL}I_d\sin\alpha$$



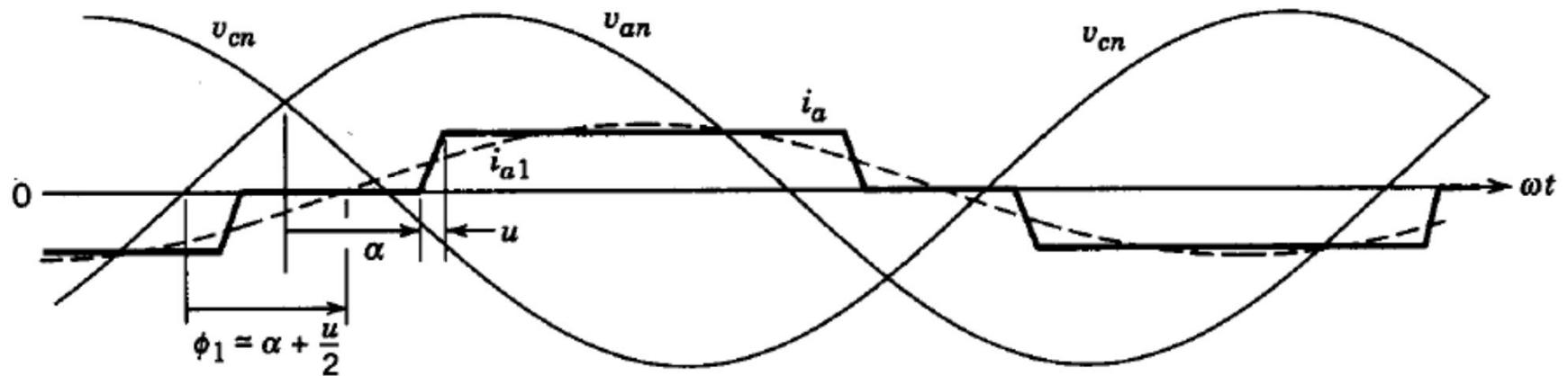
Converter with source inductance

$$V_d = \frac{3\sqrt{2}}{\pi} V_{LL} \cos \alpha - \frac{3\omega L_s}{\pi} I_d$$



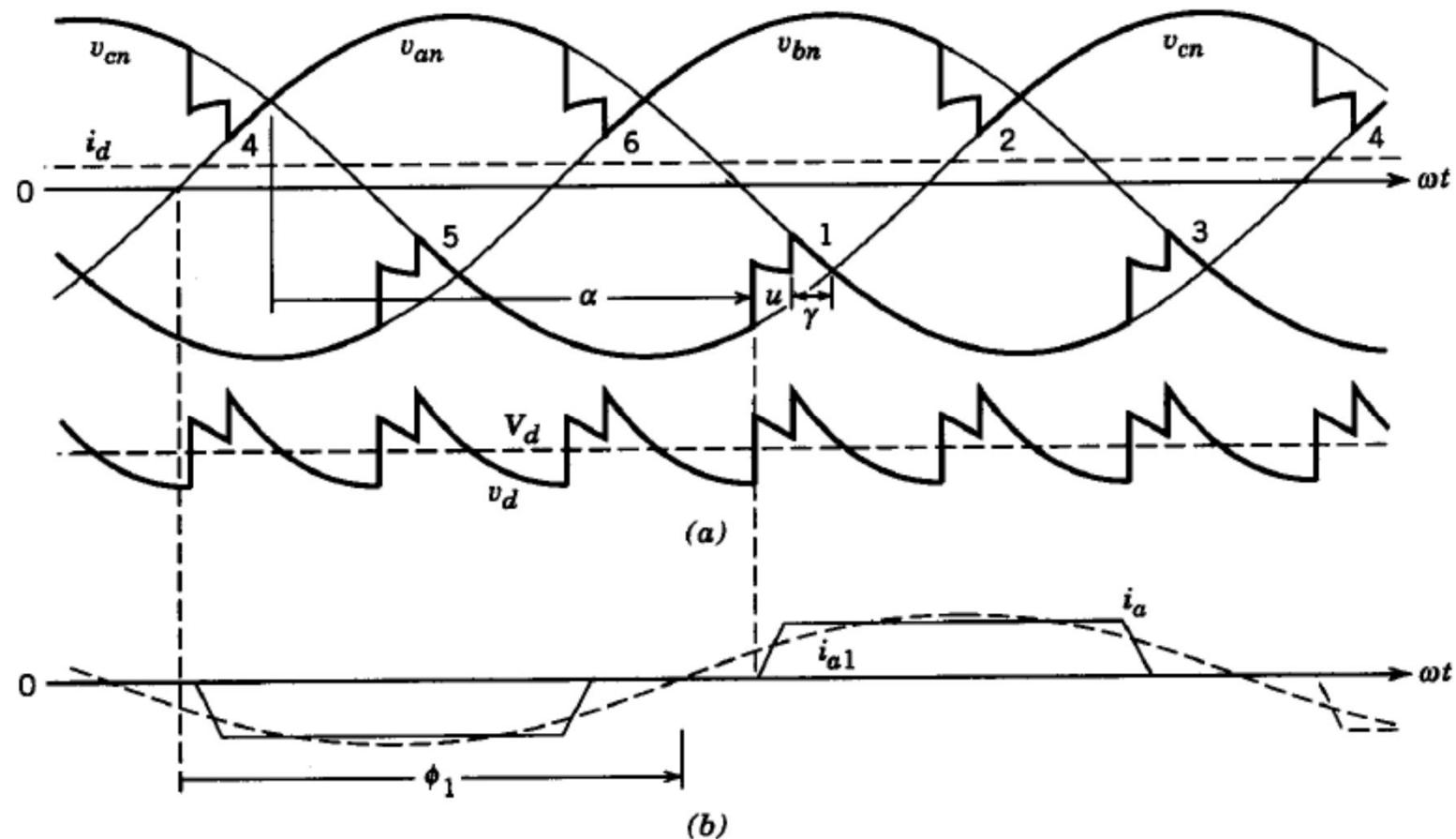
Input line current waveform

- DPF $\approx \cos(\alpha + \frac{u}{2})$



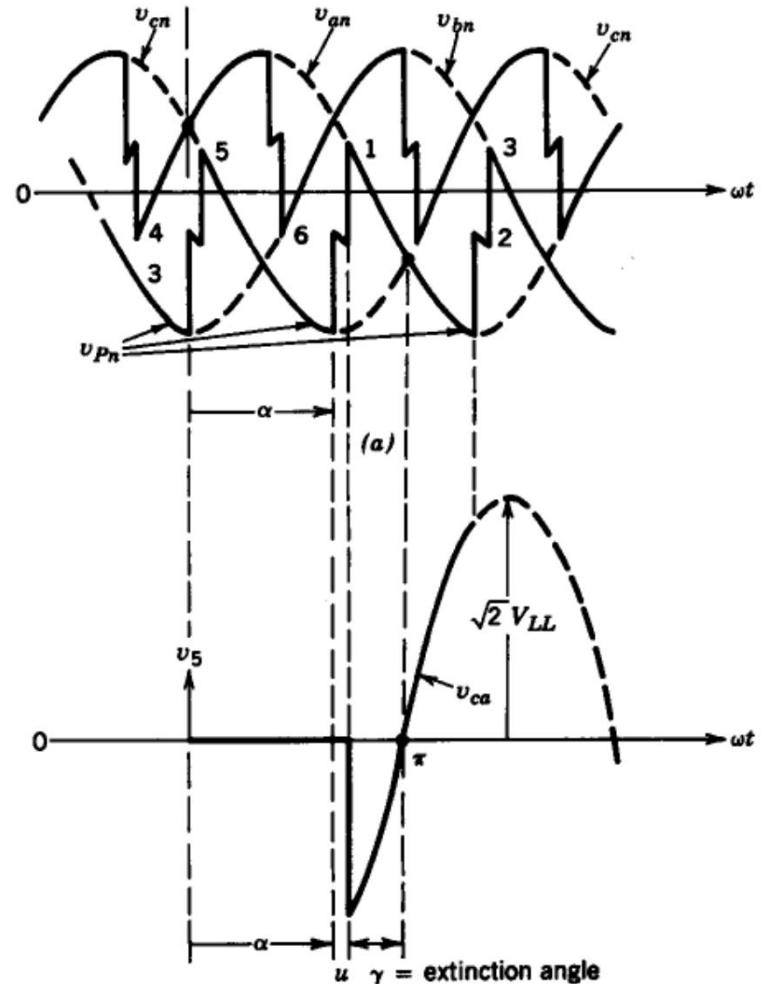
$$\cos(\alpha) - \cos(\alpha + u) = \frac{2\omega L_s}{\sqrt{2}V_{LL}} I_d$$

Inverter waveform



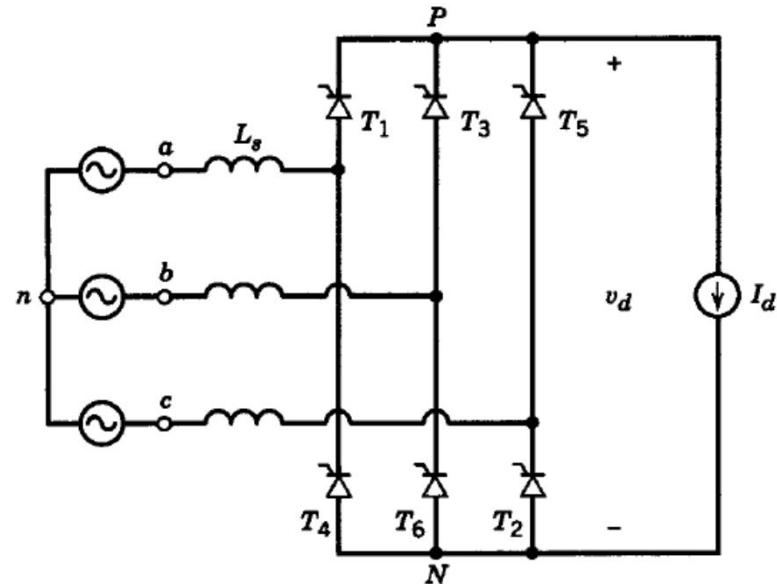
Inverter voltage over thyristor

- Extinction angle
 $\gamma = 180 - (\alpha + u)$
- Thyristor require
 $t_y = \gamma/\omega > t_q$
 (turn off time)
- Failing requirement leads to retriggering of the thyristor too early (commutation failure)
 \Rightarrow large currents (both thyristors in the same phase conducts)!

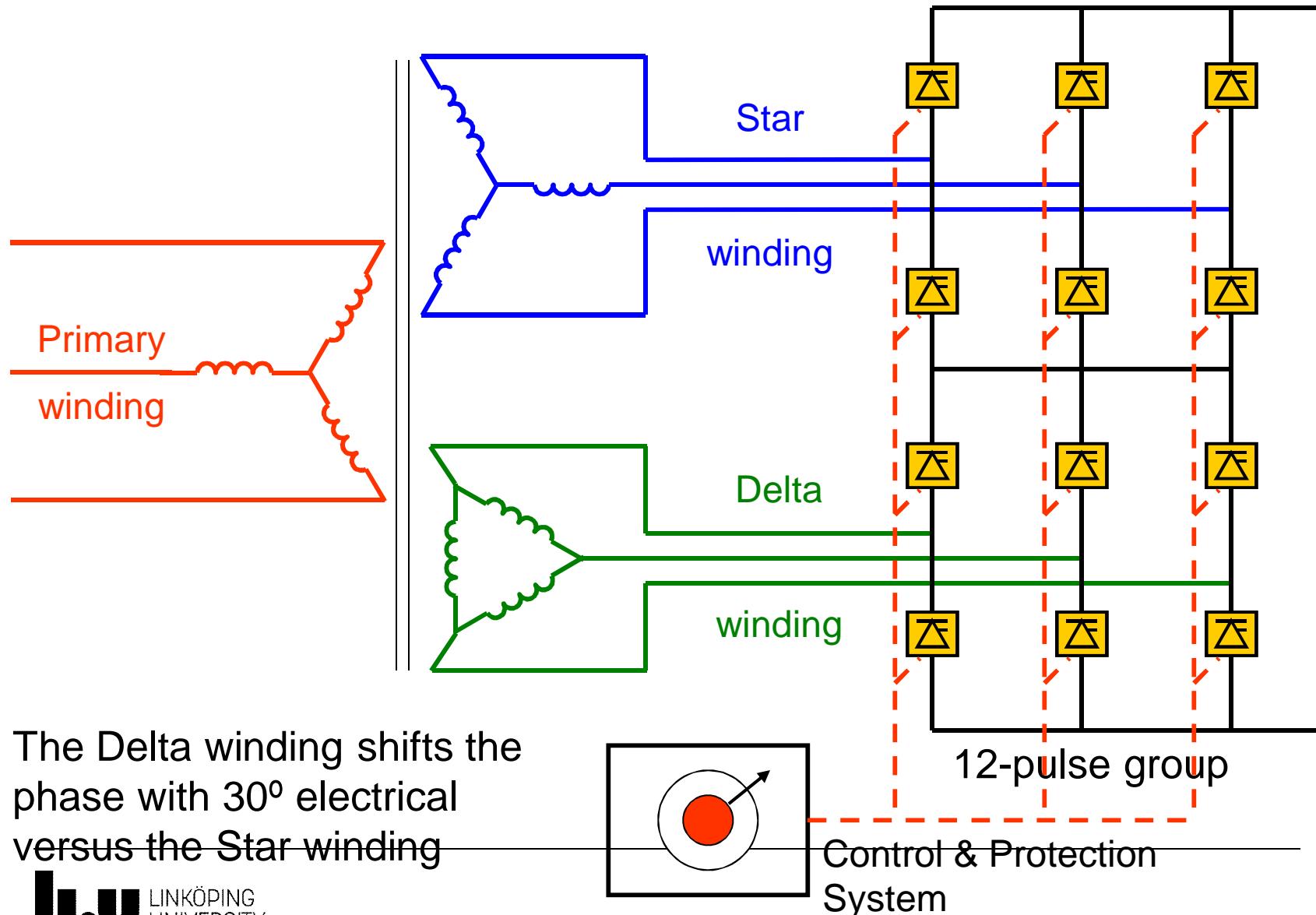


Exercise 4-101

- In the three-phase thyristor rectifier circuit with the following data:
 $V_{LL} = 400 \text{ V}$ at 50 Hz, $L_s = 7 \text{ mH}$,
 $I_d = 10\text{A}$
 - What firing angle α shall be used to get an average dc-voltage of 500V (rectifier mode)*
 - What firing angle α shall be used to get an average dc-voltage of -500V (inverter mode)*
 - Calculate γ . What minimum t_q is required?*

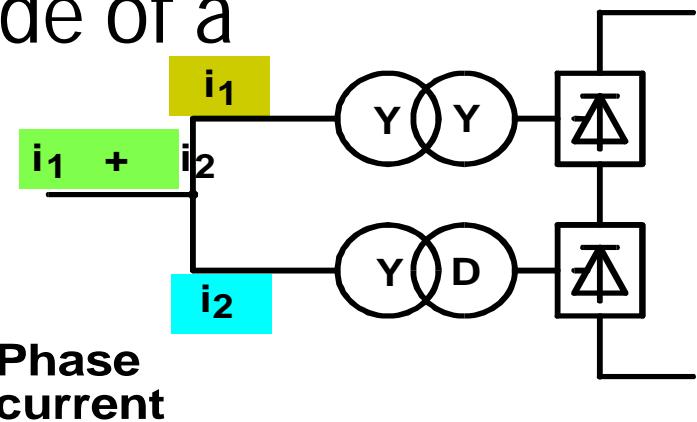
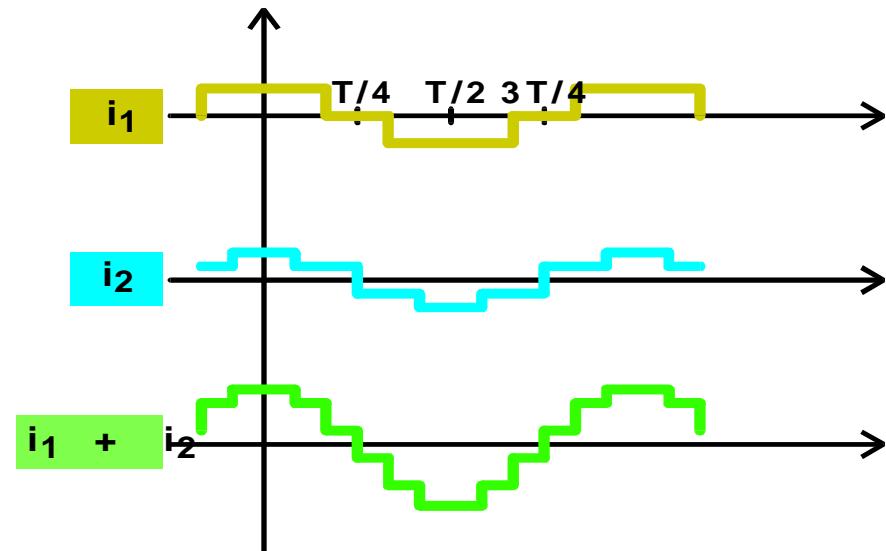


12-pulse converter

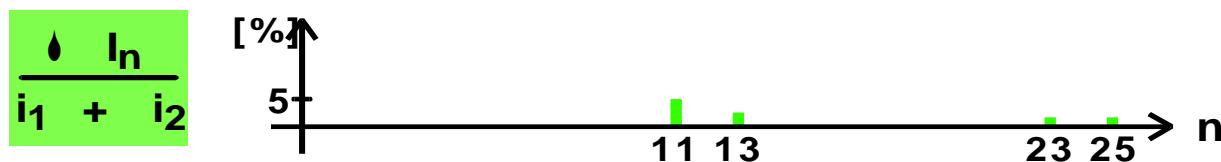
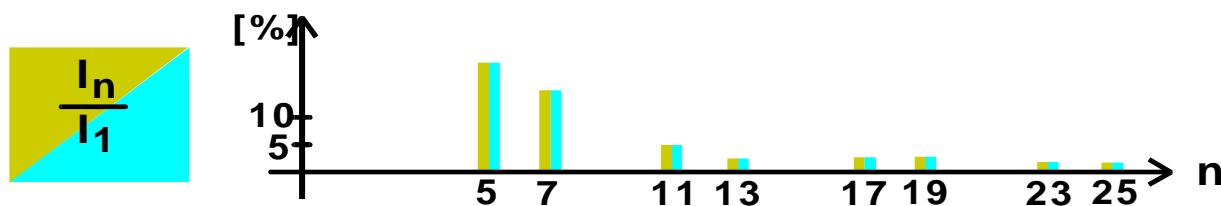


The Delta winding shifts the phase with 30° electrical versus the Star winding

Harmonic currents on the AC side of a converter



Phase current



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