

Exercises for Tutorial 4: Feedback, Stability, Frequency Compensation

- 1) Problem 10.1 in the course book.

We get a transfer function $A_{open}(s) = \frac{A_0}{\left(1 + \frac{s}{\omega_{p1}}\right)\left(1 + \frac{s}{\omega_{p2}}\right)}$, where A_0 is unknown.

The closed loop TF is $A_{closed}(s) = \frac{A_{open}(s)}{1 + \beta A_{open}(s)}$

The phase margin is defined as $PM = 180^\circ + \arg[\beta A_{open}(s = j\omega_u)]$

Since the phase margin should be 60° we can write

$$180^\circ - 60^\circ = 120^\circ = -\arg[\beta A_{open}(s = j\omega_u)] = \arctan \left[\frac{\omega_u \left(\frac{1}{\omega_{p1}} + \frac{1}{\omega_{p2}} \right)}{1 - \frac{\omega_u^2}{\omega_{p1}\omega_{p2}}} \right] \rightarrow$$

$$\omega_u \left(\frac{1}{\omega_{p1}} + \frac{1}{\omega_{p2}} \right) = \tan(120^\circ) - \tan(120^\circ) \frac{\omega_u^2}{\omega_{p1}\omega_{p2}} \rightarrow$$

$$\omega_u = -\frac{\omega_{p1} + \omega_{p2}}{2 \tan(120^\circ)} \pm \sqrt{\left(\frac{\omega_{p1} + \omega_{p2}}{2 \tan(120^\circ)} \right)^2 + \omega_{p1}\omega_{p2}} \approx 310.5 \text{ MHz}$$

$$|\beta A_{open}(s = j\omega_u)| = \frac{A_0}{\sqrt{\left(1 - \frac{\omega_u^2}{\omega_{p1}\omega_{p2}}\right)^2 + \omega_u^2 \left(\frac{1}{\omega_{p1}} + \frac{1}{\omega_{p2}}\right)^2}} = 1 \rightarrow$$

$$A_0 = \sqrt{\left(1 - \frac{\omega_u^2}{\omega_{p1}\omega_{p2}}\right)^2 + \omega_u^2 \left(\frac{1}{\omega_{p1}} + \frac{1}{\omega_{p2}}\right)^2} \approx 36.6 \approx 31.3 \text{ dB}$$

- 2) Problem 10.9 in the course book. In part (b) assume that the gain crossover point is the same as that of part (a). Also assume $\mu_n C_{ox} = 134 \mu\text{A}/\text{V}^2$, $\lambda_n = 0.1 \text{ V}^{-1}$ and $\lambda_p = 0.2 \text{ V}^{-1}$. All transistors are in saturation region.

- 3) Figure 8 shows an amplifier schematic. For simplicity we can ignore all parasitics of M_1 and M_2 . Also, we assume $g_{m1} \gg 1/r_{o1}$ and $\gamma = 0$.

- a) Determine the transfer function of the amplifier.

- b) If $g_{m1} = g_{m2} = 1 \frac{\text{mA}}{\text{V}}$, $R = r_{o2} = 20 \text{ k}\Omega$ and $C_1 = C_2 = 1 \text{ pF}$, calculate the phase margin of the circuit.

$$PM = 180^\circ + \arg(H(j\omega)), |H(j\omega)| = 1$$

$$|H(j\omega_u)| = \frac{|A_0|}{\left| \left(1 + j \frac{\omega_u}{\omega_{p1}}\right) \left(1 + j \frac{\omega_u}{\omega_{p2}}\right) \right|} = 1 \rightarrow$$

$$\omega_u^2 = x$$

$$\left(\omega_{p1}\omega_{p2} - x\right)^2 + x\left(\omega_{p1} + \omega_{p2}\right)^2 = A_0^2\left(\omega_{p1}\omega_{p2}\right)^2 \rightarrow$$

$$x = -\frac{\omega_{p1}^2 + \omega_{p2}^2}{2} \pm \sqrt{\left(A_0^2 - 1\right)\left(\omega_{p1}\omega_{p2}\right)^2 + \left(\frac{\omega_{p1}^2 + \omega_{p2}^2}{2}\right)^2} = \begin{cases} 6.11e17 \leftarrow OK \\ -1.62e18 \end{cases}$$

$$\omega_u = \pm\sqrt{x} = 781e6 \left[\frac{\text{rad}}{\text{s}} \right]$$

$$\arg(H(j\omega_u)) = \arctan \left[-\frac{\omega_u(\omega_{p1} + \omega_{p2})}{\omega_{p1}\omega_{p2} - \omega_u^2} \right] = -120.7^\circ$$

- c) Use the assumptions in part (b) to calculate the AC gain, if the input frequency is $f = \frac{1}{2\pi} \times 10^8 \text{ Hz}$

$$\omega_{in} = \omega_{p1} = 10^8 \frac{\text{rad}}{\text{s}}$$

$$\frac{\omega_{p1}}{\omega_{p2}} = \frac{10^8}{10^9} = 0.1$$

$$|H(j\omega_{p1})| = \frac{|A_0|}{\sqrt{\left(1 - \frac{\omega_{p1}}{\omega_{p2}}\right)^2 + \left(1 + \frac{\omega_{p1}}{\omega_{p2}}\right)^2}} = \frac{10}{\sqrt{0.9^2 + 1.1^2}} = \frac{10}{\sqrt{2.02}} \approx 7$$

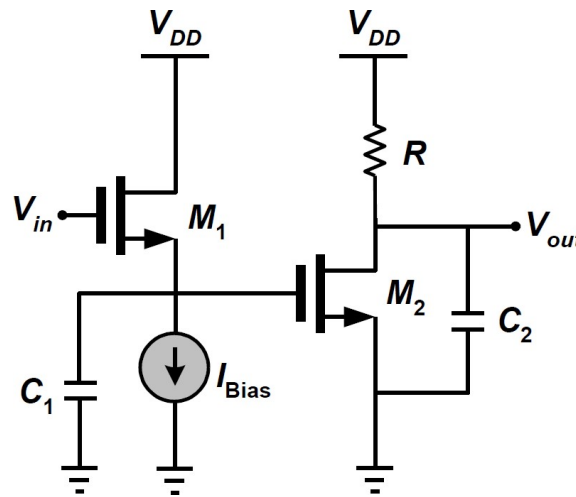


Figure 8 An amplifier schematic.

- 4) Figure 9 shows an amplifier schematic. For simplicity we can ignore all parasitics of M_1 and M_2 . Also we assume $\lambda = 0$.

- a) Determine the transfer function of the amplifier.
b) If the amplifier behaves like a single-pole system, show $g_{m2}R = 1$.

$$g_{m2}R = 1$$

$$\frac{V_{out}}{V_{in}} = -\frac{g_{m1}R(1+sC_1R)}{(1+sC_1R)(1+sC_2R)} = -\frac{g_{m1}R}{1+sC_2R}, \text{ where } \omega_p = \frac{1}{C_2R}$$

- c) If $g_{m1} = g_{m2} = 0.32 \frac{\text{mA}}{\text{V}}$, $R = 5 \text{ k}\Omega$, $C_1 = 0.2 \text{ pF}$ and $C_2 = 1 \text{ pF}$, calculate the phase shift through the amplifier circuit for an input signal with $f = 143.3 \text{ MHz}$.

$$\omega_{in} = 2\pi f_{in} = 2\pi 143.3e6 \left[\frac{\text{rad}}{\text{s}} \right]$$

$$H(j\omega) = -\frac{g_{m1}}{(g_{m2} - \omega^2 RC_1 C_2)^2 + [\omega(C_1 + C_2)]^2} \left([g_{m2} + \omega^2 C_1^2 R] + j\omega [RC_1(g_{m2} - \omega^2 C_1 C_2 R) - C_1 + C_2] \right)$$

$$\arg(H(j\omega)) = \arctan\left[\frac{\omega[RC_1(g_{m2} - \omega^2 RC_1 C_2) - C_1 - C_2]}{g_{m2} + \omega^2 C_1^2 R}\right] \approx -72.4^\circ$$

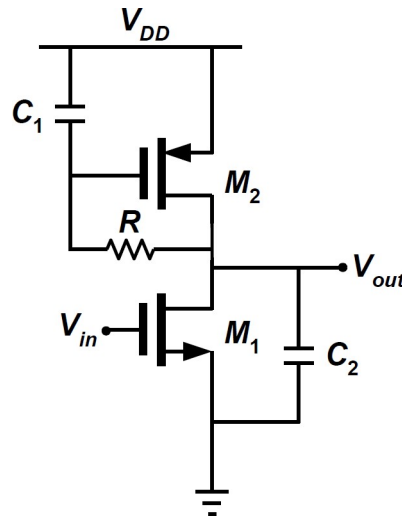


Figure 9 An amplifier schematic.

- 5) An amplifier circuit has two poles at $100 \frac{\text{Mrad}}{\text{s}}$ and $500 \frac{\text{Mrad}}{\text{s}}$, with no zeros. Calculate the DC gain of the amplifier to get a phase margin of 90° .

$$\arg(H(j\omega)) = \arctan\left[-\frac{\omega_u(\omega_{p1} + \omega_{p2})}{\omega_{p1}\omega_{p2} - \omega_u^2}\right] = -90^\circ$$

$$-\frac{\omega_u(\omega_{p1} + \omega_{p2})}{\omega_{p1}\omega_{p2} - \omega_u^2} = \tan(-90^\circ) \approx -\infty \rightarrow$$

$$\omega_{p1}\omega_{p2} - \omega_u^2 \approx 0 \rightarrow \omega_u = \sqrt{\omega_{p1}\omega_{p2}} \approx 224 \frac{\text{Mrad}}{\text{s}}$$

$$|H(j\omega_u)| = \left| \frac{A_0 \omega_{p1} \omega_{p2}}{(\omega_{p1}\omega_{p2} - \omega_u^2) + j\omega_u(\omega_{p1} + \omega_{p2})} \right| = 1 \rightarrow$$

$$A_0 = \frac{\sqrt{(\omega_{p1}\omega_{p2} - \omega_u^2)^2 + \omega_u^2(\omega_{p1} + \omega_{p2})^2}}{\omega_{p1}\omega_{p2}} = \frac{\sqrt{0^2 + \omega_u^2(\omega_{p1} + \omega_{p2})^2}}{\omega_{p1}\omega_{p2}} =$$

$$\frac{\omega_u(\omega_{p1} + \omega_{p2})}{\omega_{p1}\omega_{p2}} = \frac{\omega_u(\omega_{p1} + \omega_{p2})}{\omega_u^2} = \frac{\omega_{p1} + \omega_{p2}}{\omega_u} = \frac{\omega_{p1} + \omega_{p2}}{\sqrt{\omega_{p1}\omega_{p2}}} \approx 2.68 \approx 8.6 \text{ dB}$$

- 6) Figure 10 shows a source-follower circuit. For simplicity we can ignore all parasitics. Also we assume $\lambda = 0$.

a) Determine the transfer function of the circuit.

b) If $g_{m1} = 1 \frac{\text{mA}}{\text{V}}$, $R = 10 \text{ k}\Omega$, $C_1 = 1 \text{ pF}$ and $C_2 = 0.1 \text{ pF}$, calculate the AC gain and the phase shift through the source-follower circuit for an input frequency of $5 \frac{\text{Grad}}{\text{s}}$.

$$|H(j\omega_{in})| = \frac{\sqrt{1 + \left(\omega_{in} \frac{C_1(1 + g_m R)}{g_m}\right)^2}}{\sqrt{\left(1 - \omega_{in}^2 \frac{RC_1 C_2}{g_m}\right)^2 + \left(\omega_{in} \frac{C_1(1 + g_m R) + C_2}{g_m}\right)^2}} \approx \frac{55.0}{60.47} \approx 0.91$$

$$\arg(H(j\omega_{in})) = \arctan \left[\frac{\omega_{in} \left((1 + g_m R) C_1 (g_m - \omega_{in}^2 RC_1 C_2) - g_m ((1 + g_m R) C_1 + C_2) \right)}{g_m^2 - \omega_{in}^2 g_m R C_1 C_2 + \omega_{in}^2 (1 + g_m R) C_1 ((1 + g_m R) C_1 + C_2)} \right]$$

$$\approx \arctan \left[-\frac{0.013755}{0.0030285} \right] \approx 24.4^\circ$$

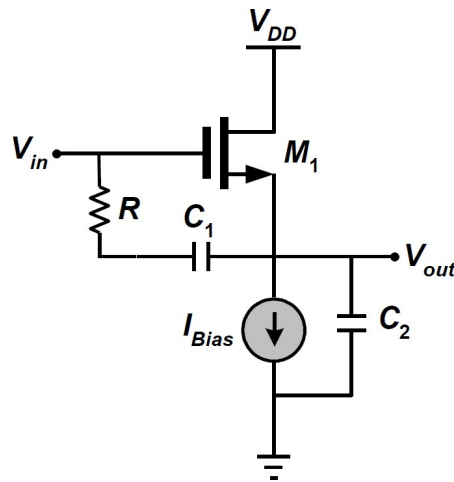


Figure 10 Source follower