

# TSTE19 Power Electronics

- Lecture 9
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  - ISY/EKS

# Outline

- Blanking time
- Gate and base driver circuits
- Analysis of full-bridge switching (Lab 2 prep)

# Blanking time effects

- Avoid cross-conduction by delay of device turn-on (blanking time)
- Polarity dependent
- Independent on output magnitude

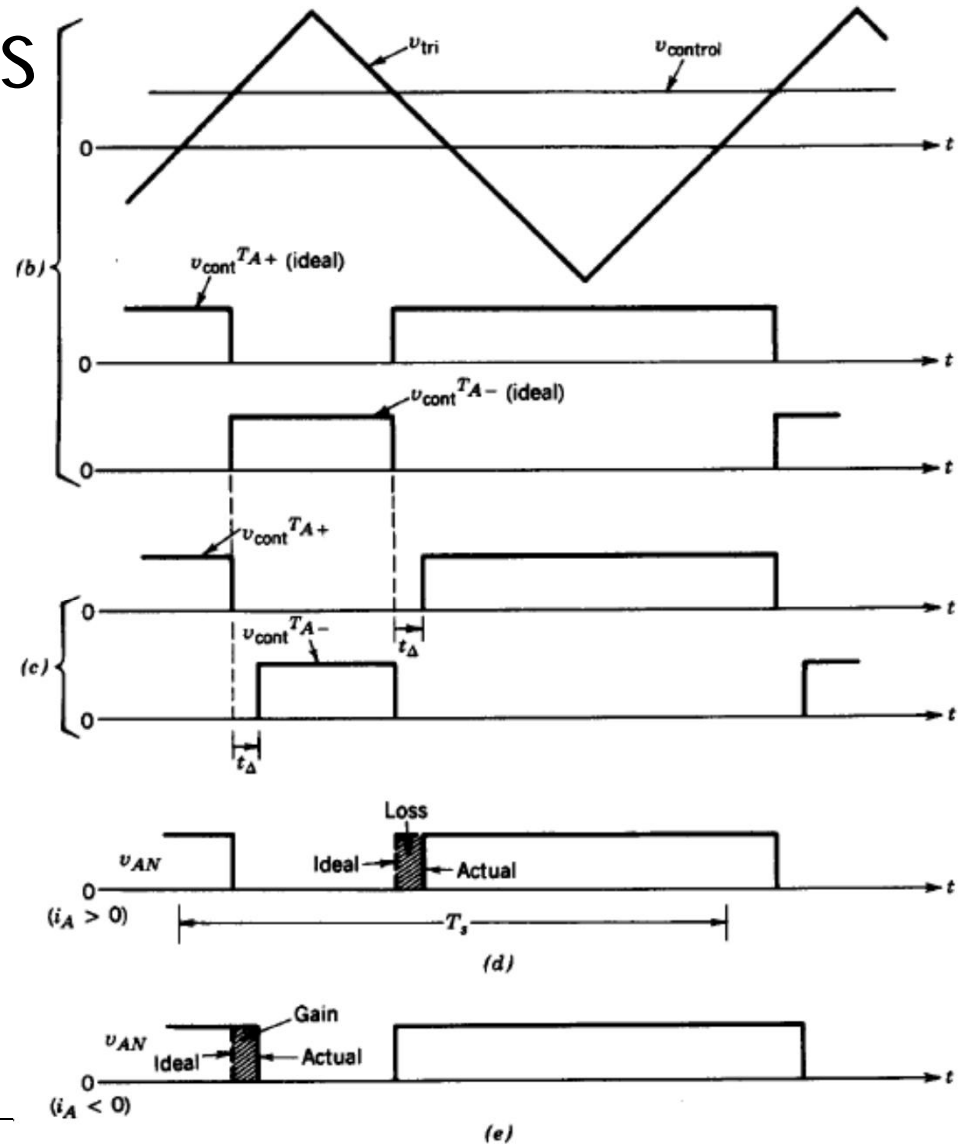
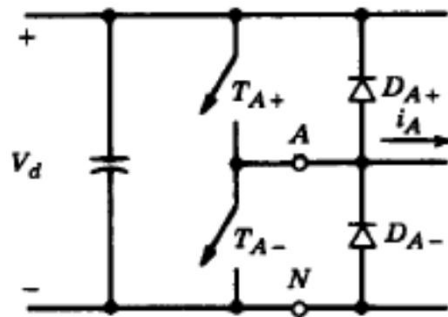
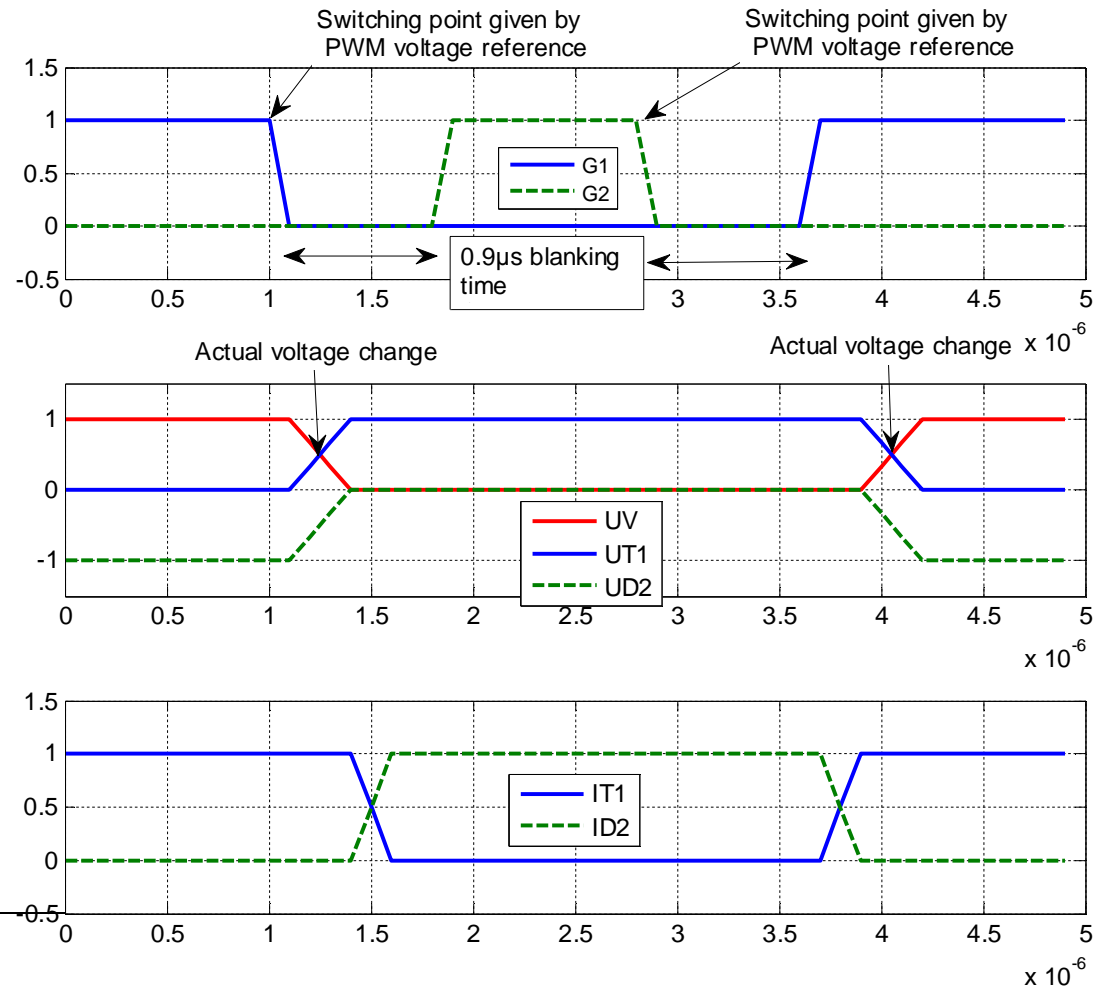


Figure 8-31 Effect of blanking time  $t_{\Delta}$ .

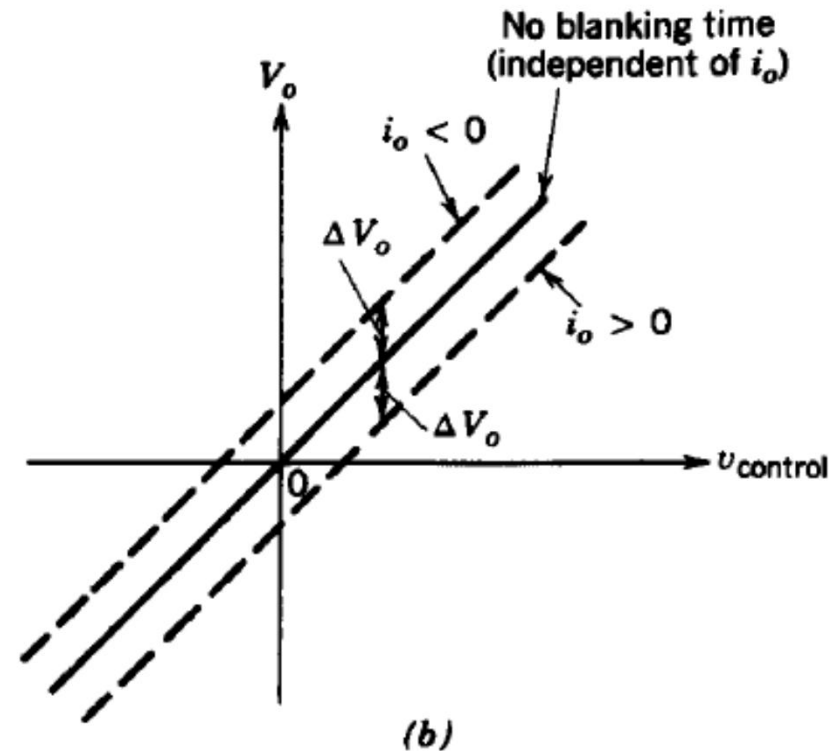
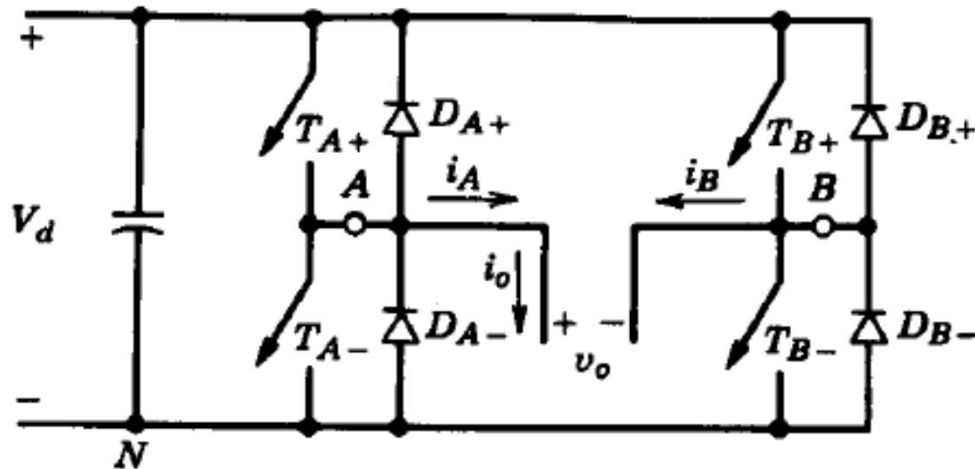
# Blanking time effects 2

- Switching points defined by the PWM reference and triangular carrier crossing
- Actual voltage change delayed by blanking time

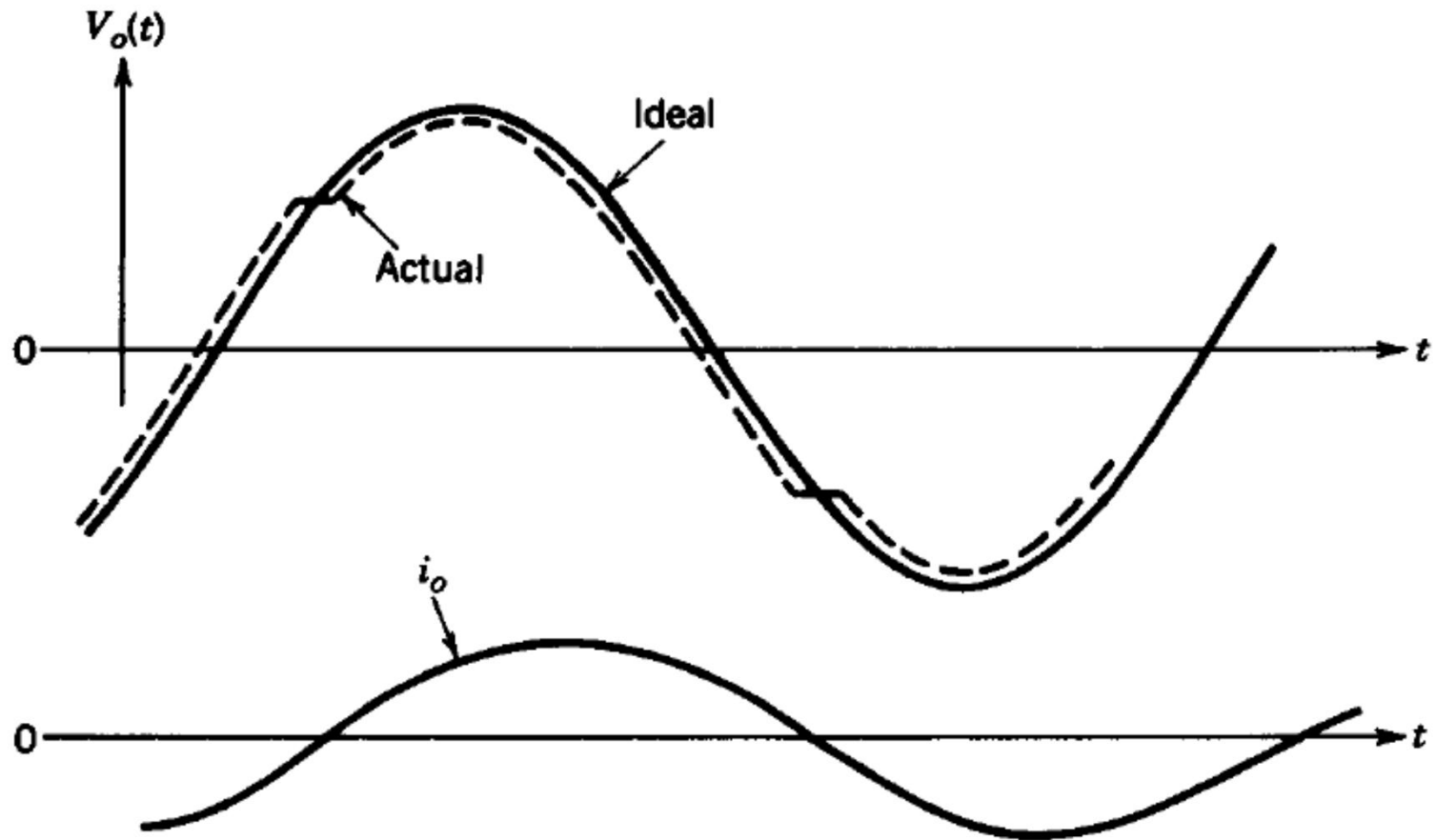


# Blanking time effect on $V_o$

- Current polarity dictates error polarity



# Blanking effect on sinusoidal output

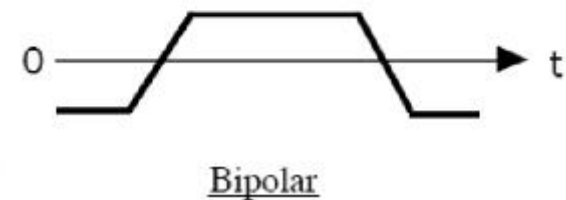


# Gate and base driving circuits

- Minimize turn-on and turn-off times
  - Avoid spending time in active region with large  $V$  and  $I$
- Controllable switches have often low current or voltage amplification factors
  - $B$  in range of 5-10 for power BJTs
  - Must supply enough energy to keep switch on
- Protect from overvoltage and/or overcurrent conditions
- Electric insulation from control logic

# Driver circuit design

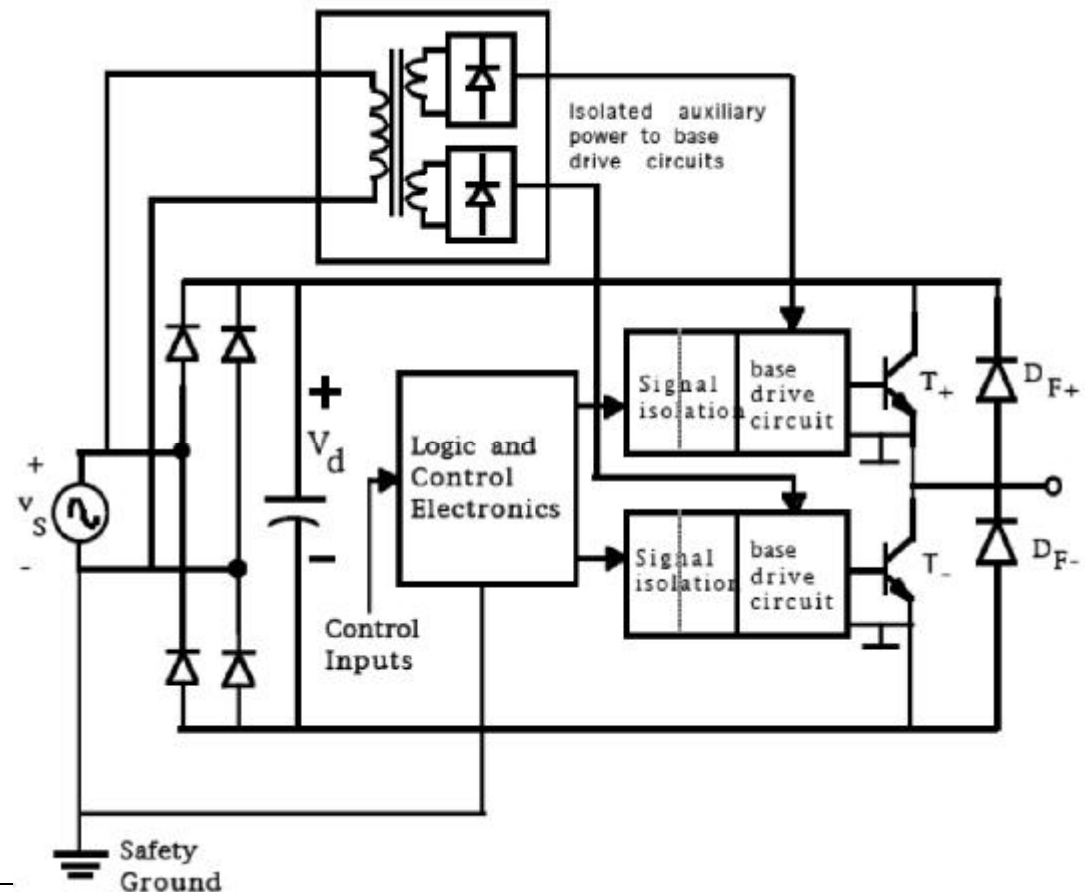
- Driver circuit topologies
  - Unipolar vs bipolar output signal to gate
  - AC or DC coupled
  - Shunt or series with power switch
- Gate current magnitude
  - Large  $I_{gon}$  shorten turn-on time but lengthen turn
  - Large  $I_{goff}$  shorten turn-off time but lengthen turn-on time
- Overcurrents, blanking time in bridge configurations
- Waveshaping for better switch performance
  - $di/dt$  for diode turn-off
  - $dv/dt$
  - Speedup capacitors





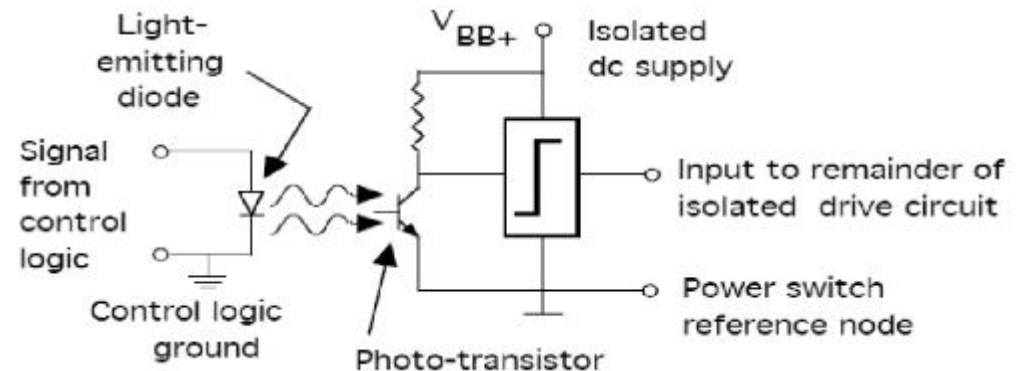
# Electrical isolation of drive circuit

- $V_d$  – potential varies with input  $v_s(t)$  relative to safety ground
- Signal isolation to base drive circuit necessary

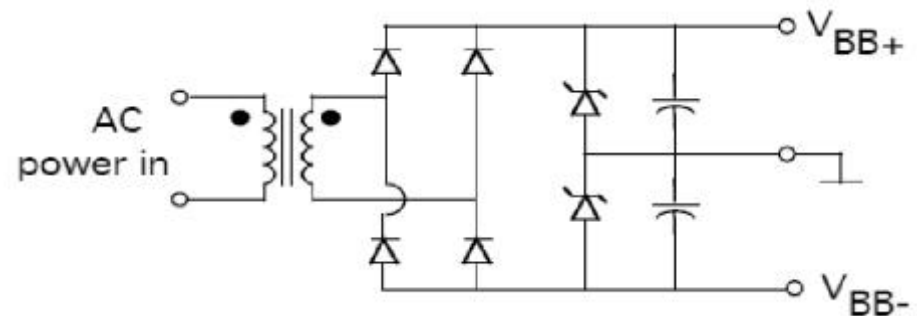


# Isolation methods for gate drive

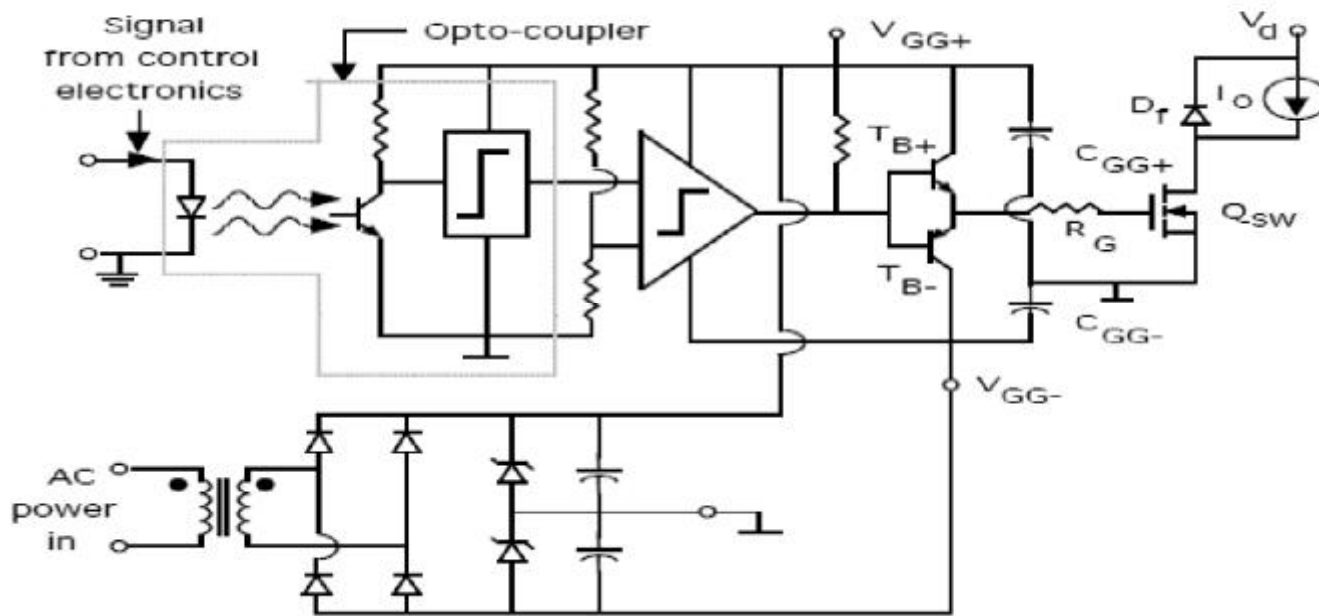
- Optical isolation of control signals
  - Opto-coupler
  - Optical fiber



- Transformer isolation
  - Isolated dc power supply for drive circuits
- Independent supply
  - Supply derived from voltage or current locally at the switch

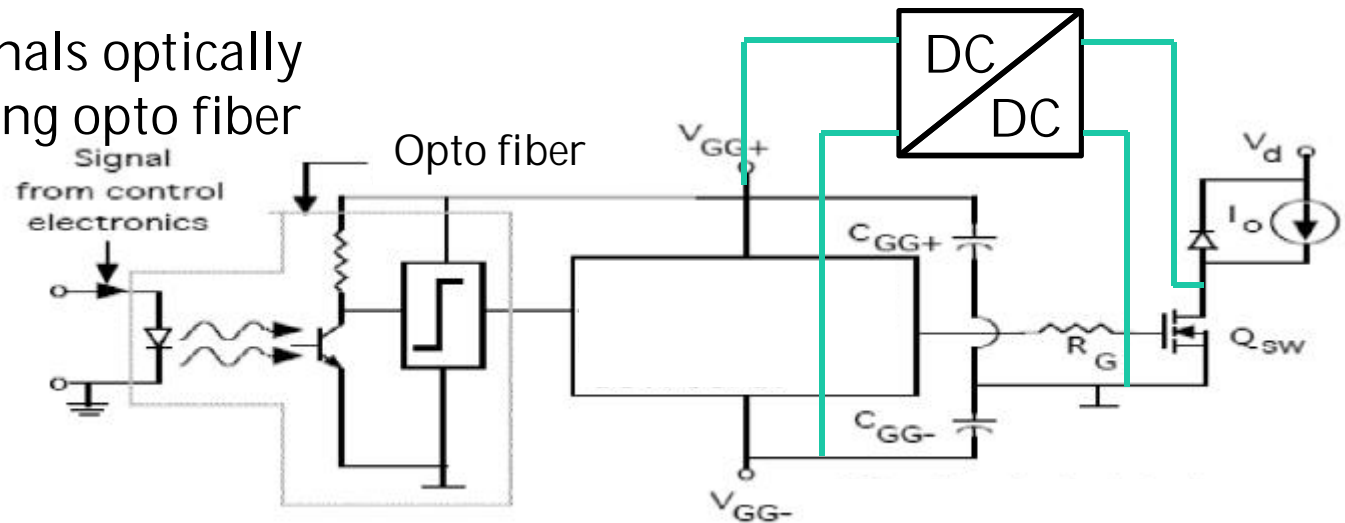


# Optocoupler isolated MOSFET



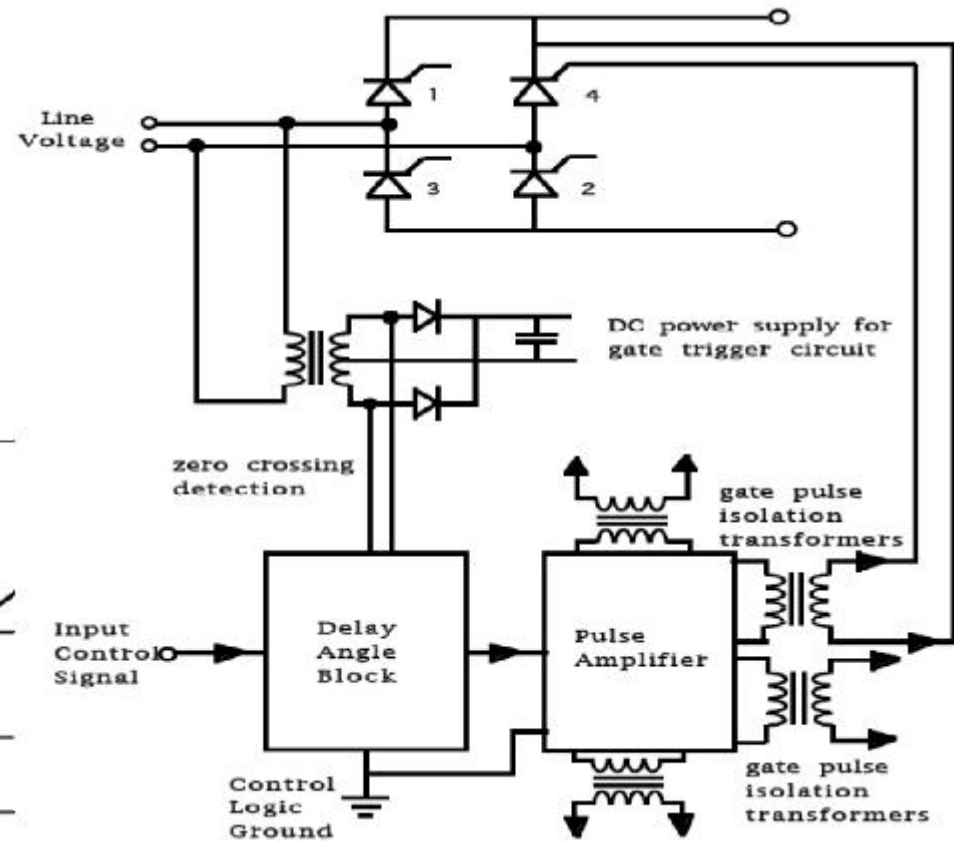
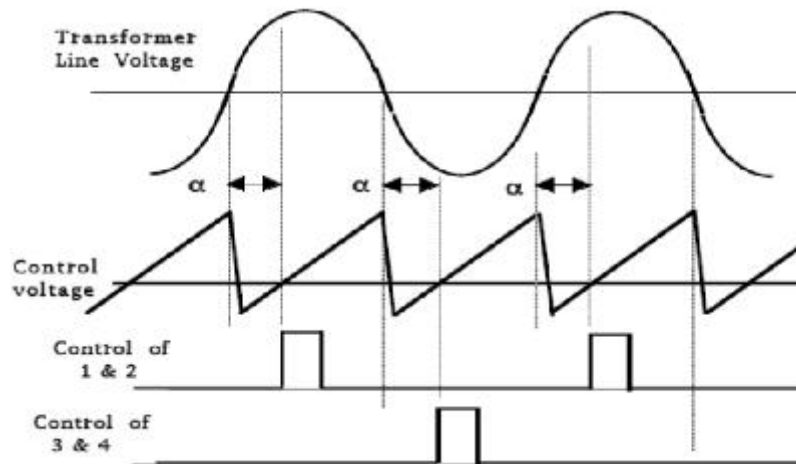
# Independent gate drive supply

- Independent gate drive supply for high isolation voltage requirements
  - Supply derived from voltage across  $Q_{sw}$
- Control signals optically isolated using opto fiber

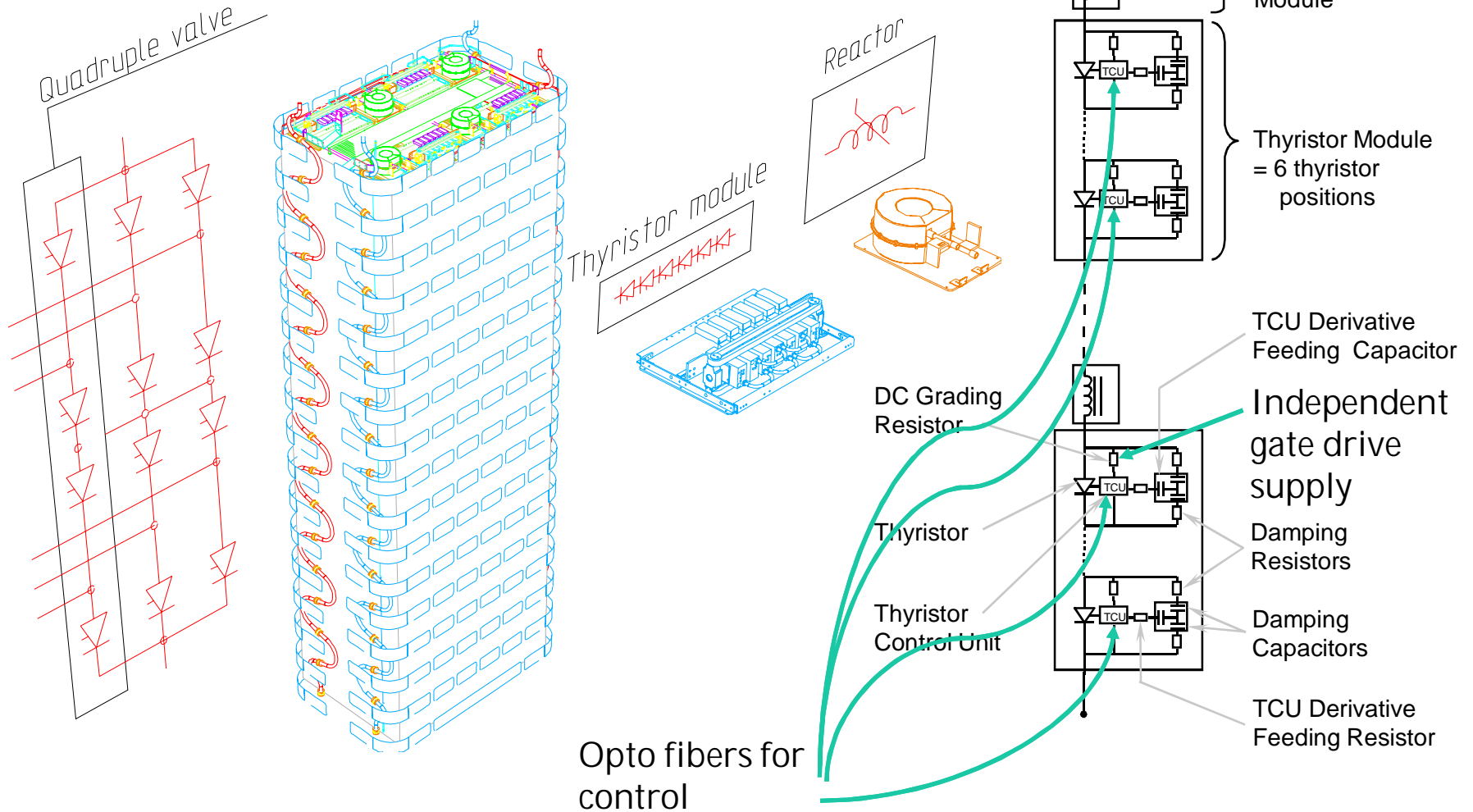


# Thyristor gate drive circuit

- Gate pulses through pulse isolation transformers

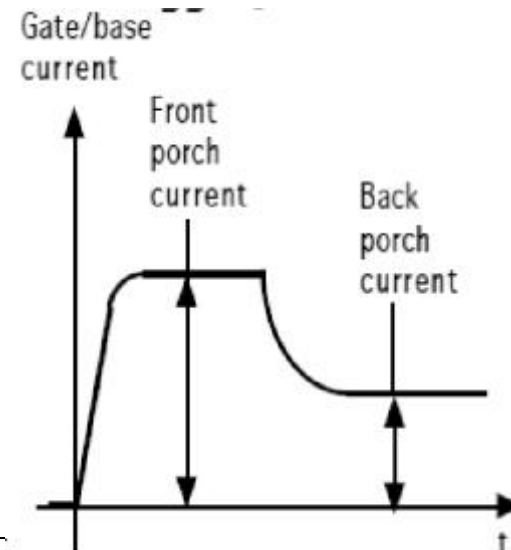
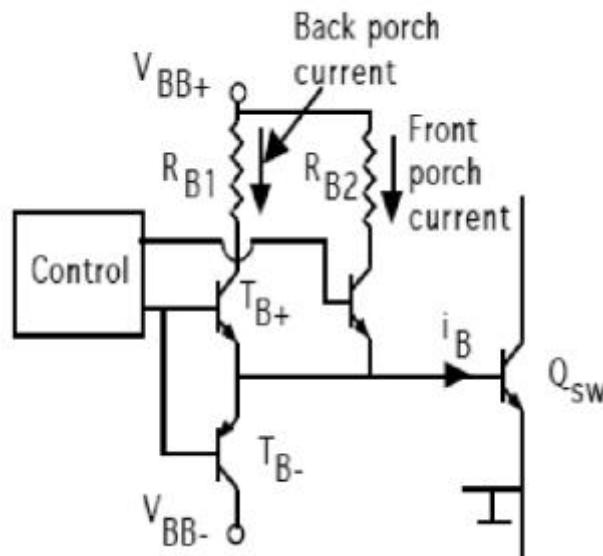


# HVDC Valve Layout

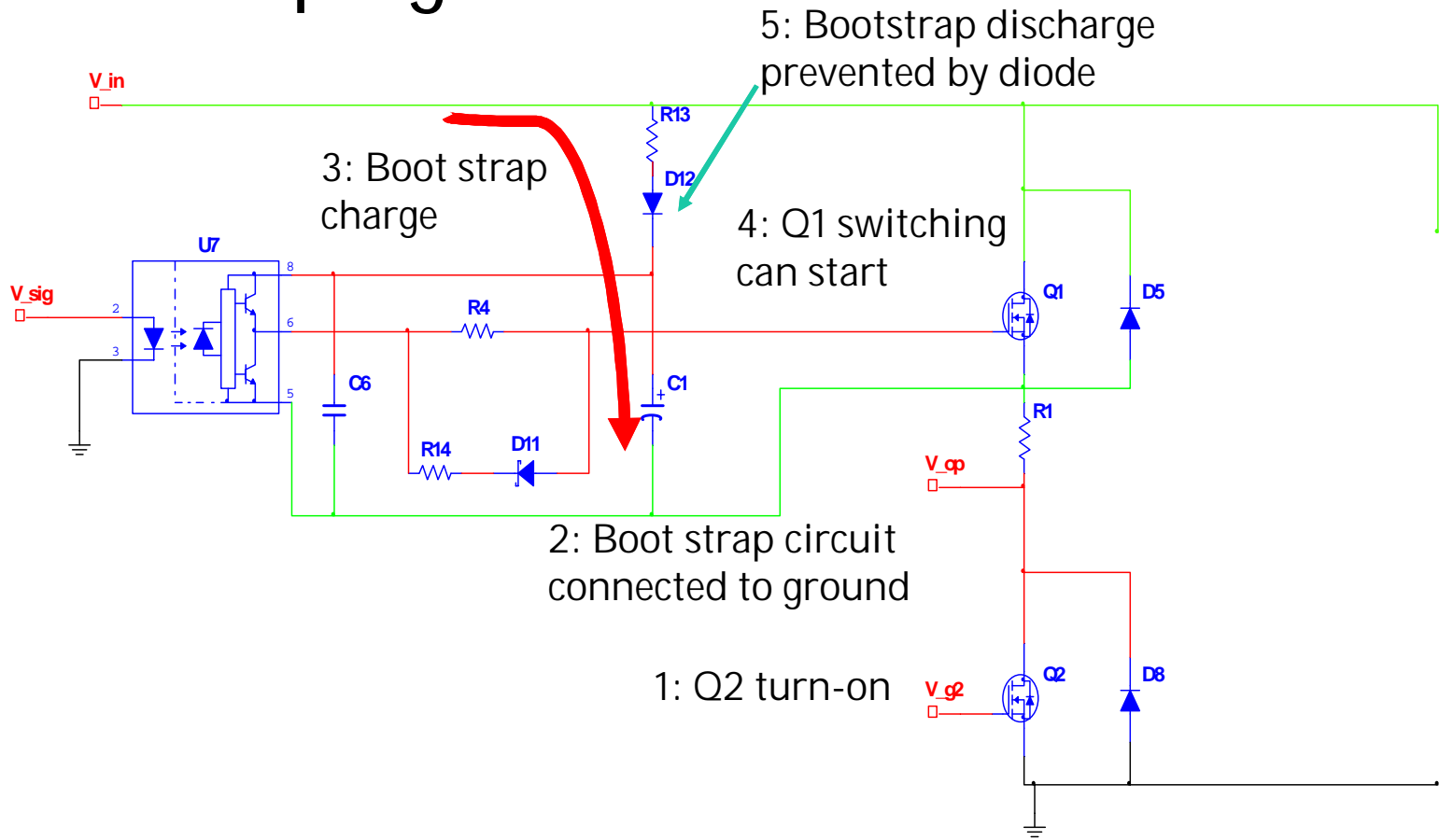


# Drive circuit waveshaping

- Drive turn-on harder, then reduce base current at end of pulse
  - Increase turn-on speed, without increasing turn-off time

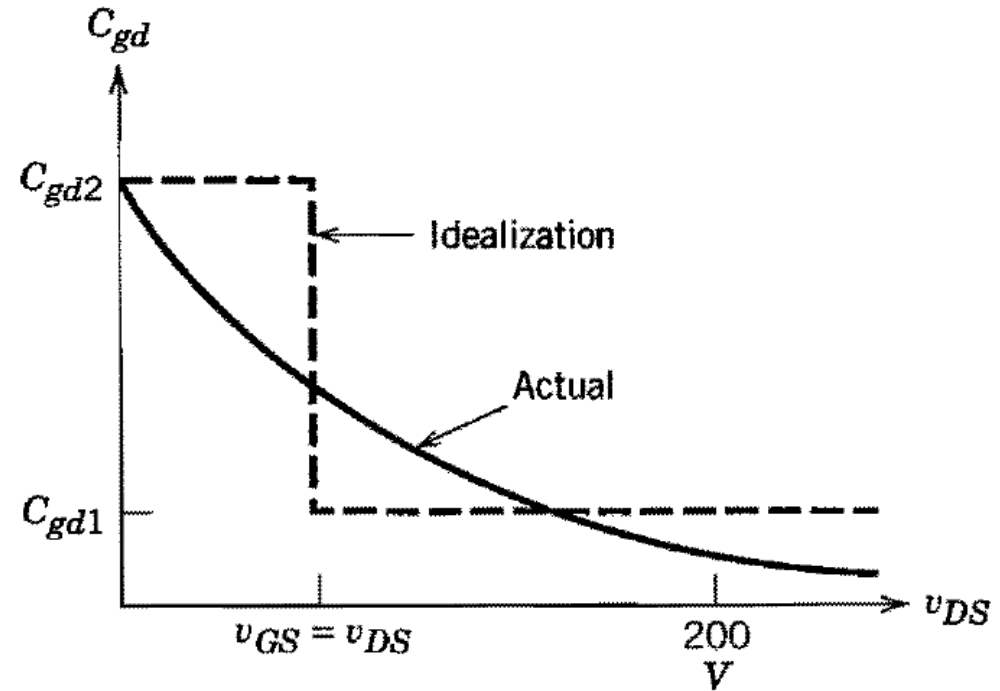
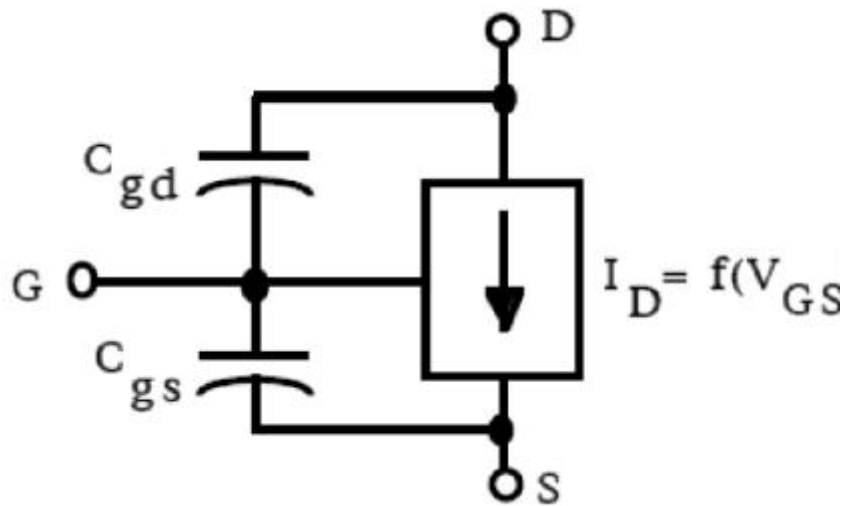


# Bootstrapping



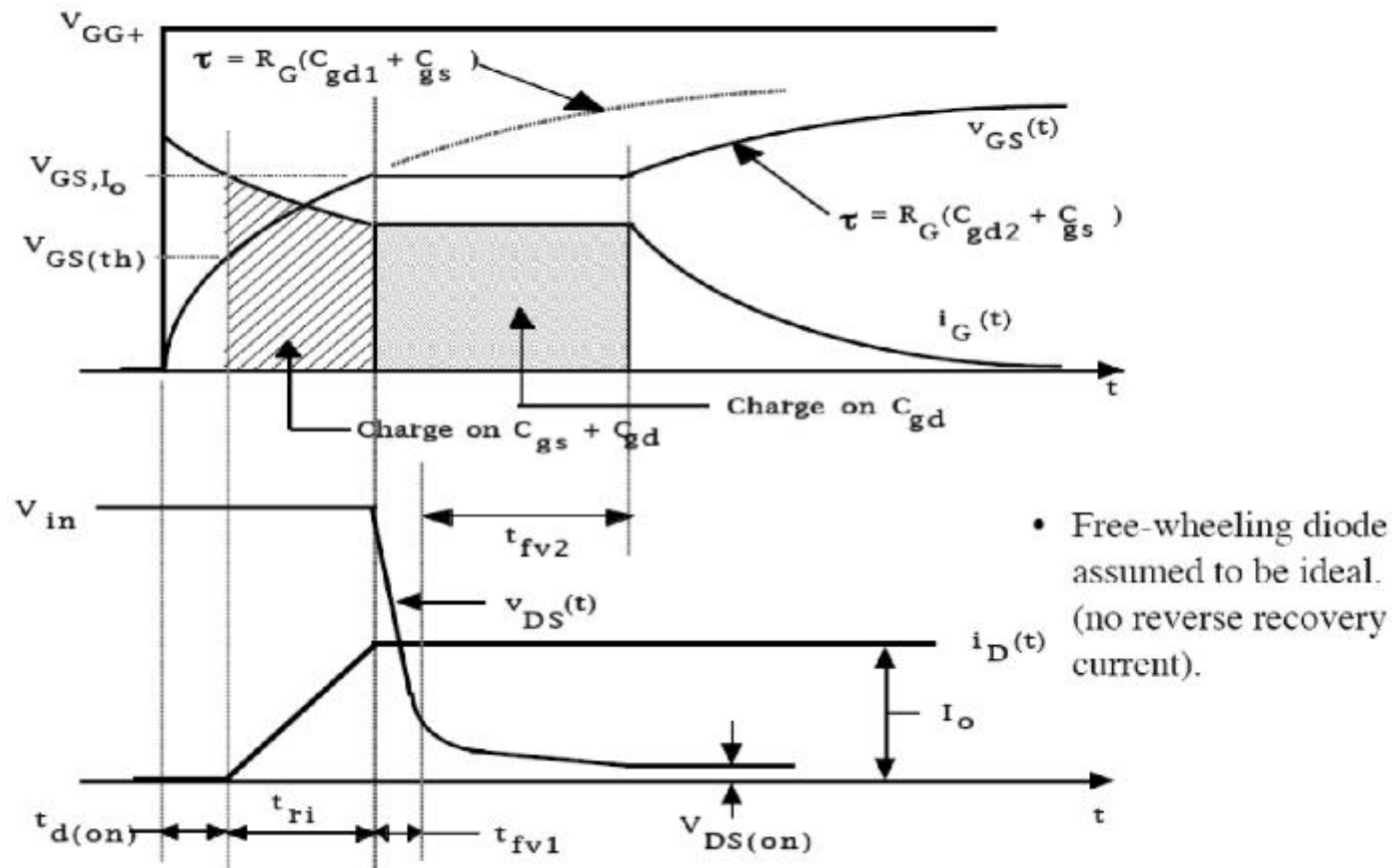


# MOSFET turn-on/turn-off equivalent

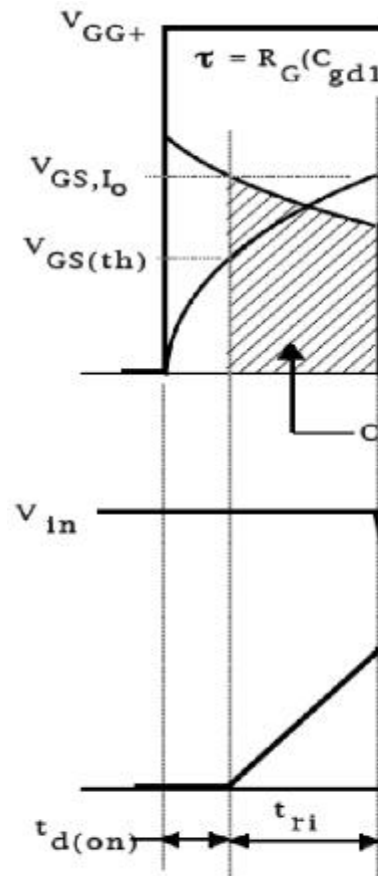


- MOSFET equivalent circuit valid for off-state (cutoff) and active region operation.

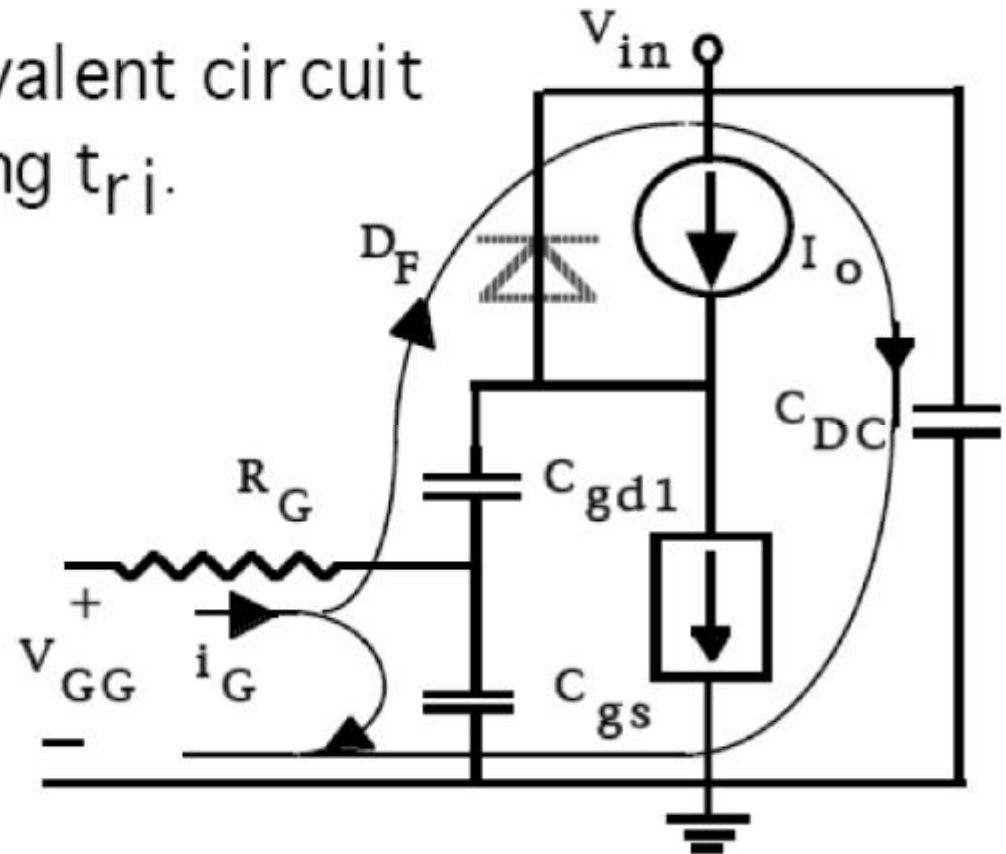
# MOSFET (IGBT) turn-on wave forms



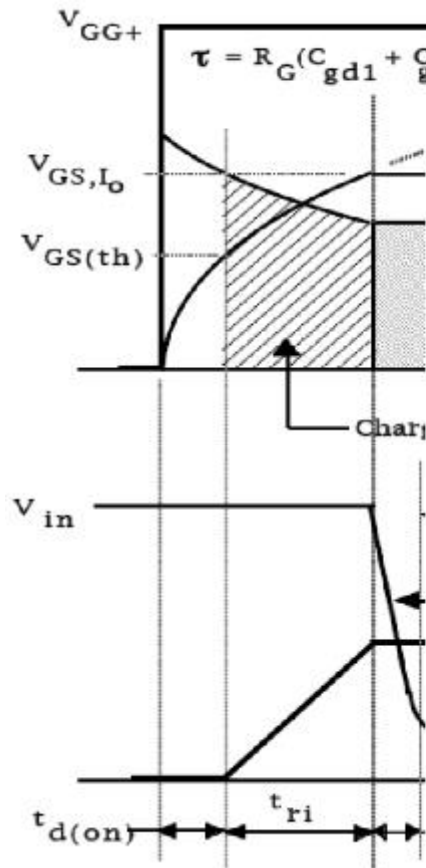
# MOSFET (IGBT) turn-on wave forms



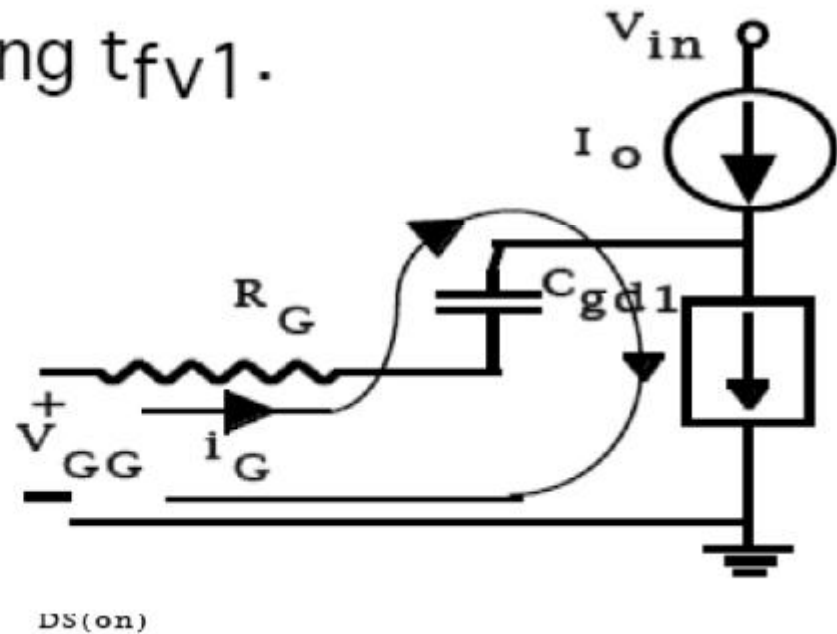
• Equivalent circuit during  $t_{ri}$ .



# MOSFET (IGBT) turn-on wave forms

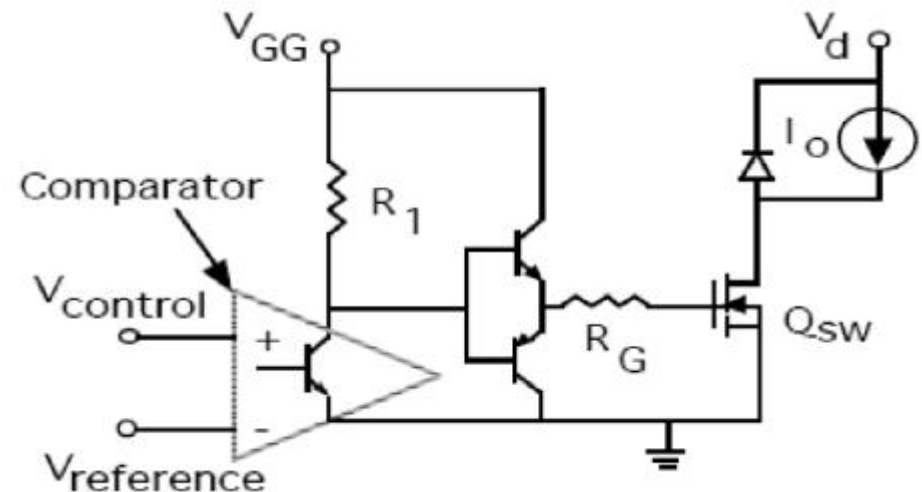
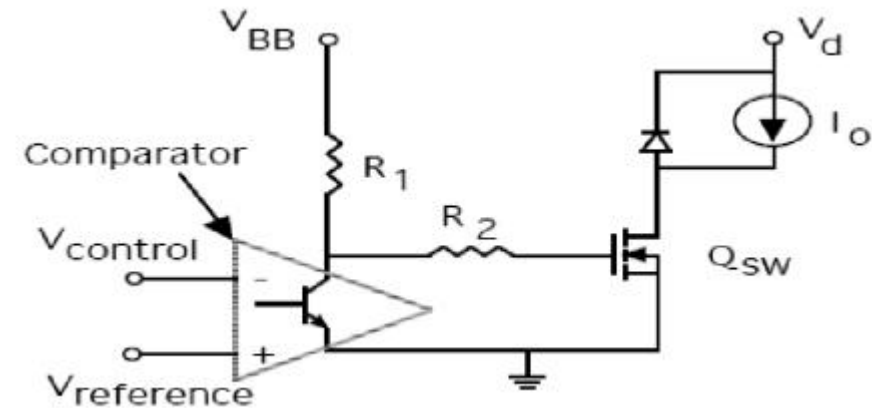


- Equivalent circuit during  $t_{fv1}$ .



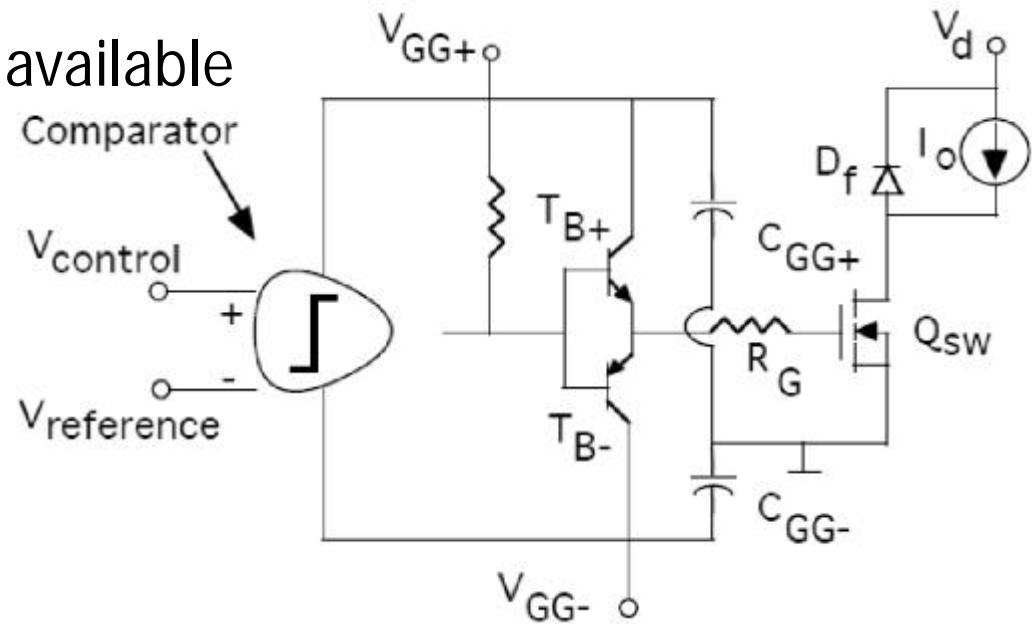
# Unipolar DC-coupled driver MOSFET examples

- Simple MOSFET gate drive
  - Gate have large parasitic capacitance
  - $R_1$  large due to  $V_{BB}/R_1$  flowing when switch off
  - $R_1$  limit turn-on time
  
- npn-pnp totem-pole stack
  - $R_G$  can be small, only used to charge/discharge parasitic capacitance in switch
  - Integrated circuits available with same function

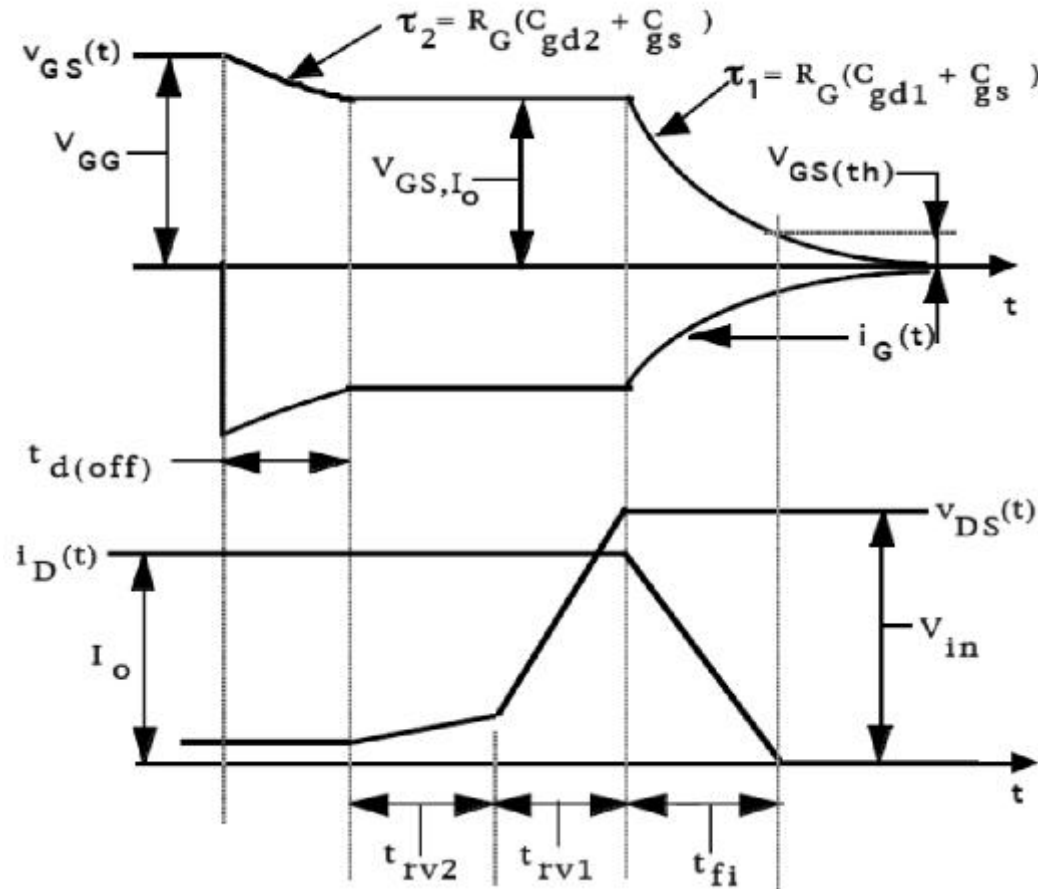


# Bipolar DC-coupled Driver MOSFET example

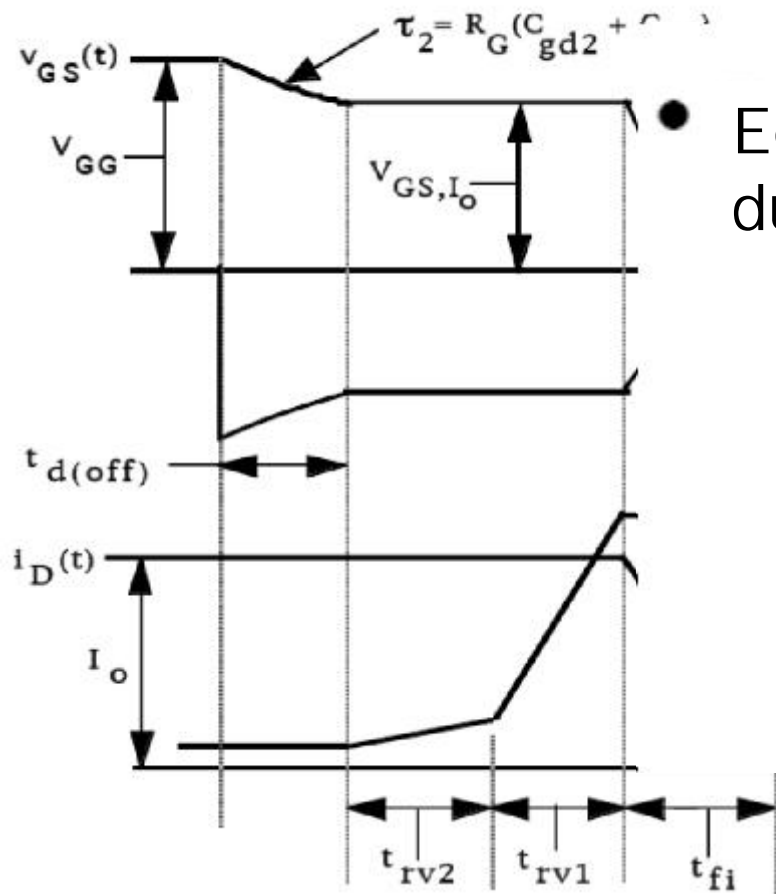
- $T_{B+}$  and  $T_{B-}$  help charge/discharge gate capacitance of  $Q_{SW}$
- $R_G$  can be small
- Integrated circuits also available



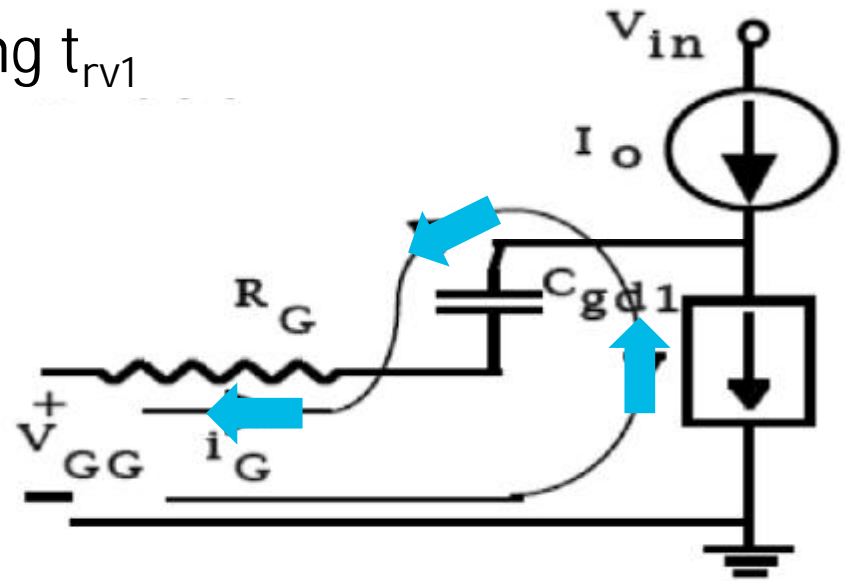
# MOSFET (IGBT) turn-off wave forms



# MOSFET (IGBT) turn-off wave forms



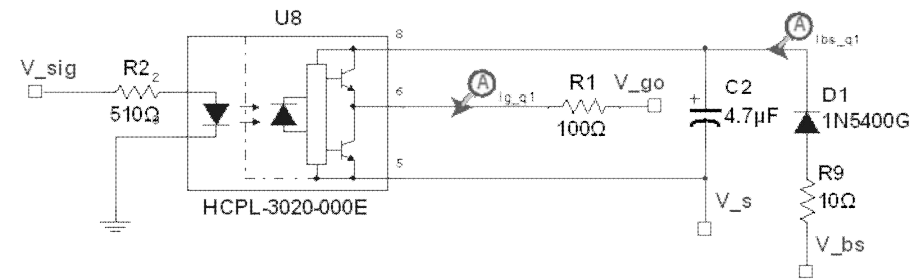
● Equivalent circuit during  $t_{rv1}$



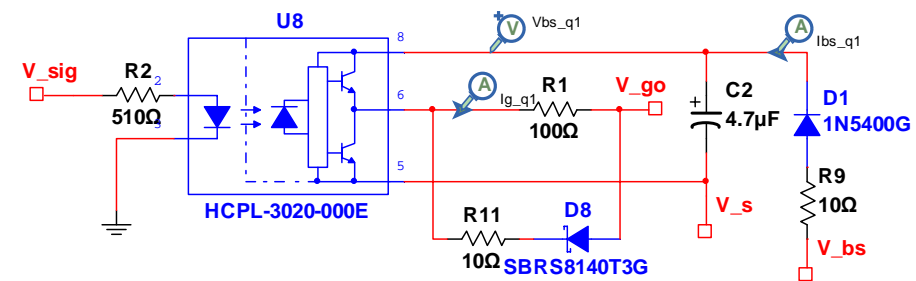


# Gate resistance control

- Separate  $R_{g\text{on}}$  and  $R_{g\text{off}}$
- Reduced  $R_{g\text{off}}$  to prevent paracitic turn-on at high  $dv/dt$



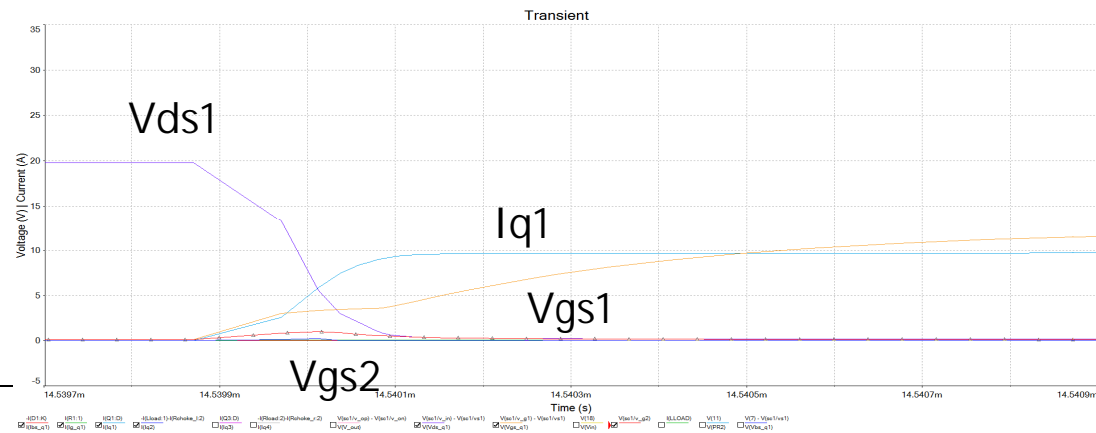
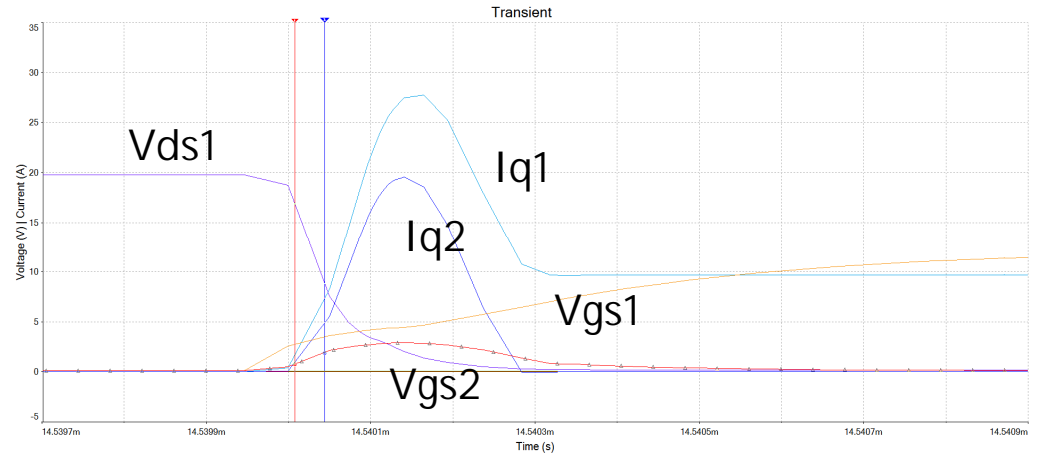
$R_g = 100$  ohm both for turn-on and turn-off



$R_g = 100$  ohm for turn-on and  
10 ohm for turn-off

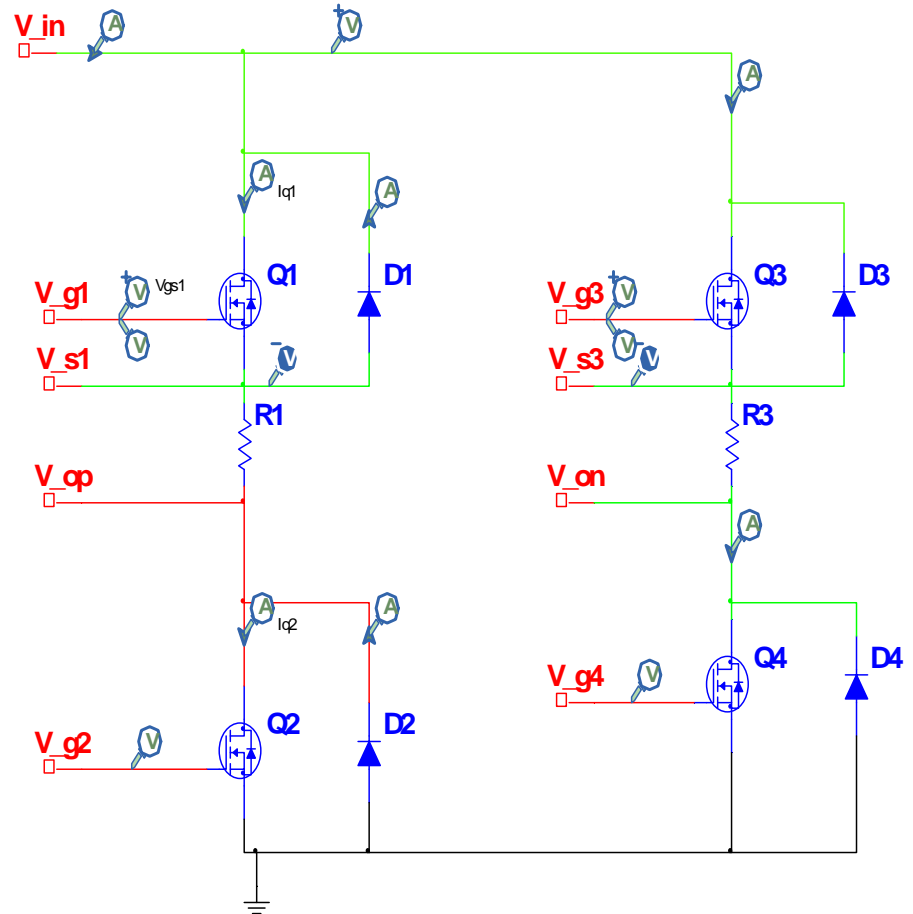
# Gate resistance control 2

- $R_{gon} = 100 \text{ ohm}$ ,  
 $R_{goff} = 100 \text{ ohm}$
- $R_{gon} = 100 \text{ ohm}$ ,  
 $R_{goff} = 10 \text{ ohm}$   
schottky SBRS8140

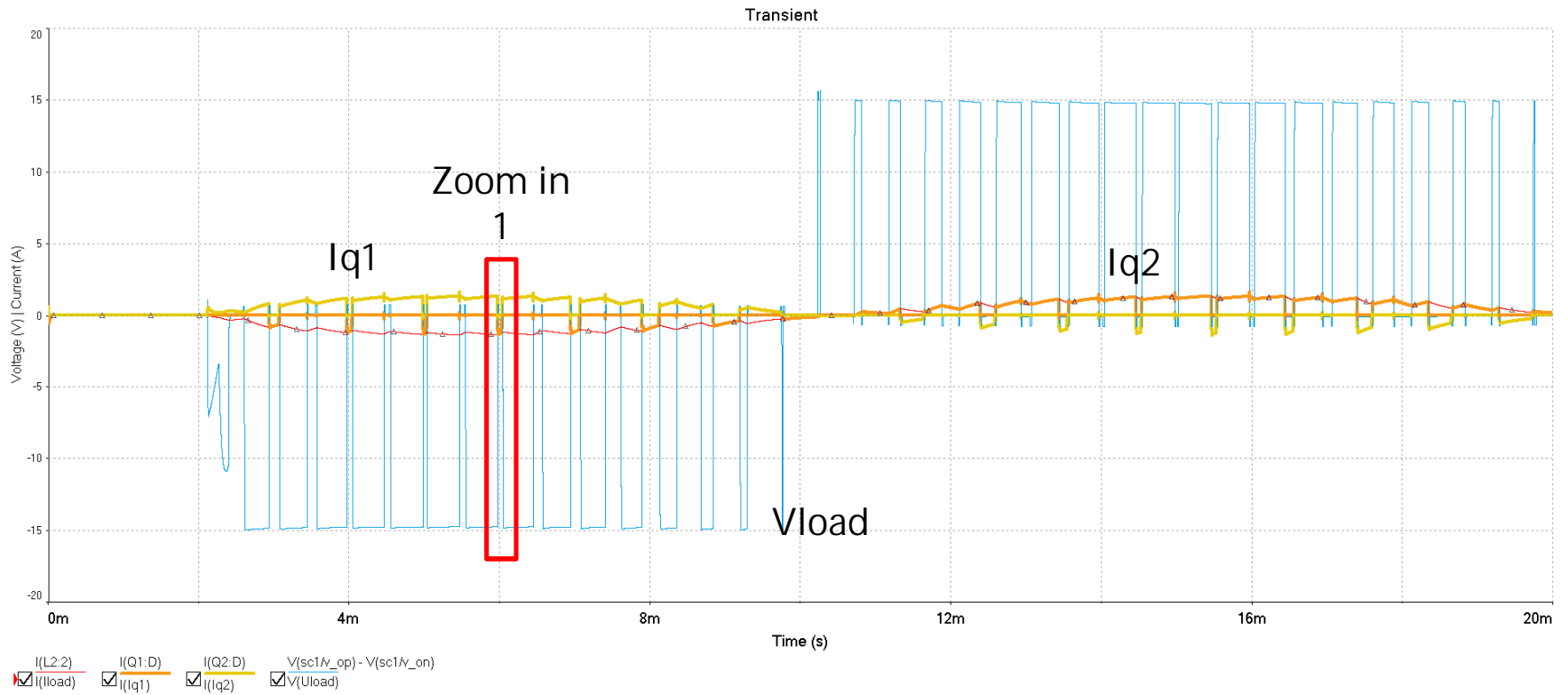


# Full-bridge inverter

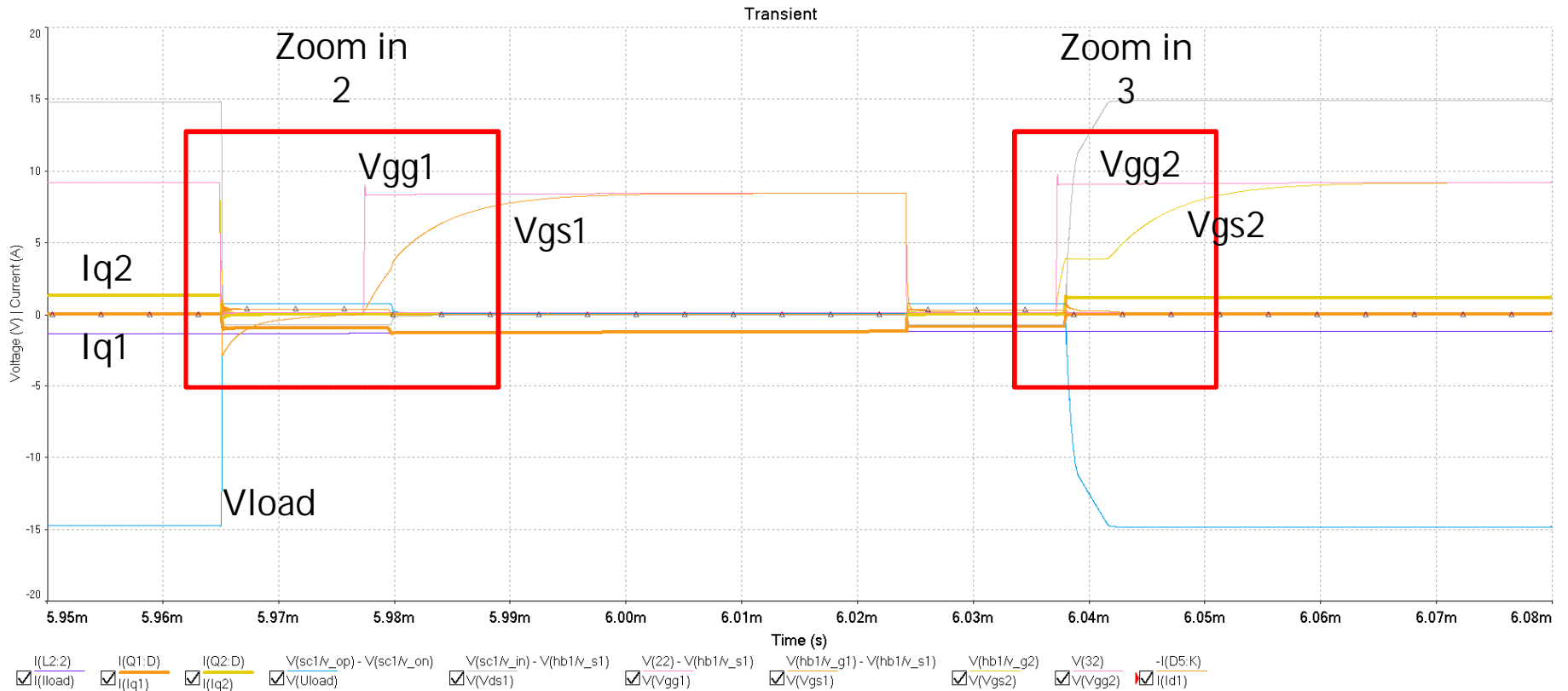
- Output voltage:  
 $V_{load} = V_{op} - V_{on}$
- Load: Resistance and inductance



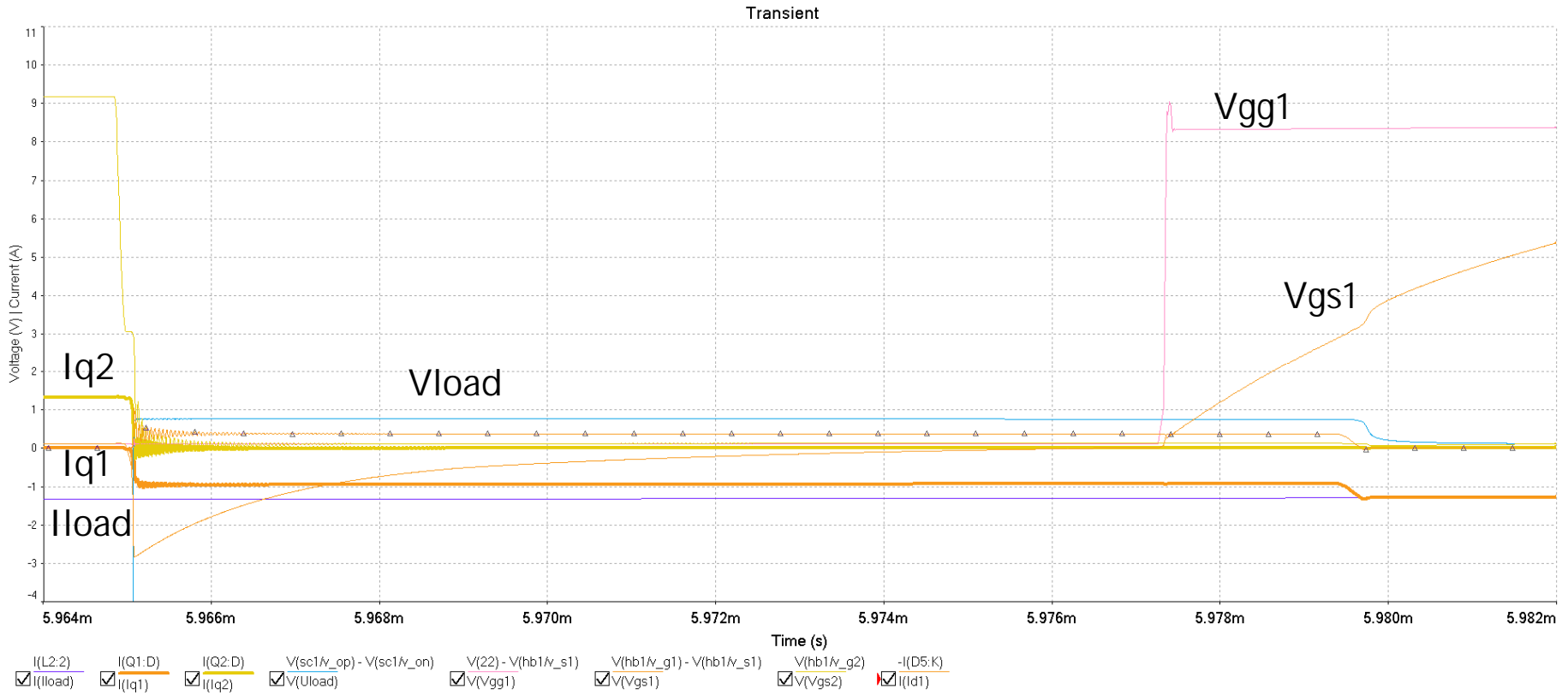
# Unipolar switching, full 20ms cycle



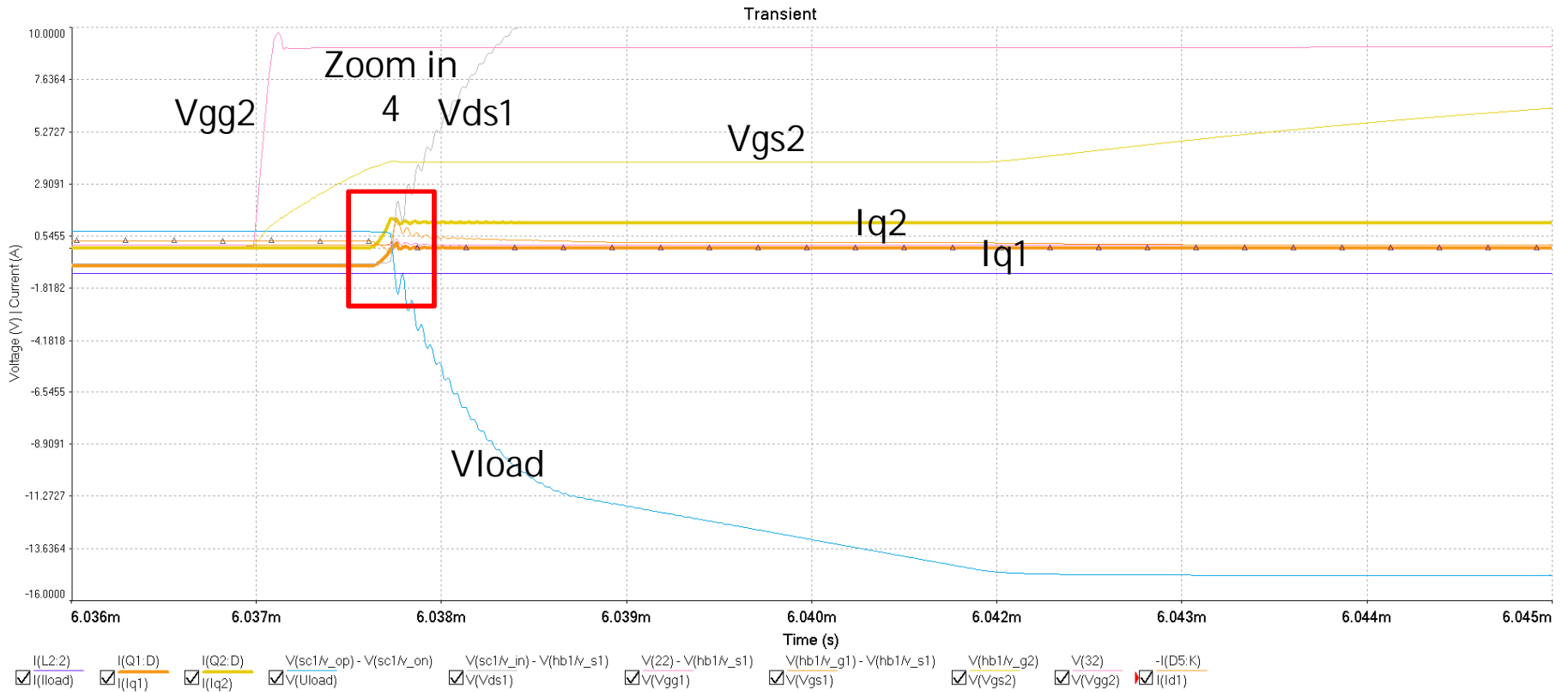
# Zoom in 1: Q2 off – Q1 on – Q1 off – Q2 on



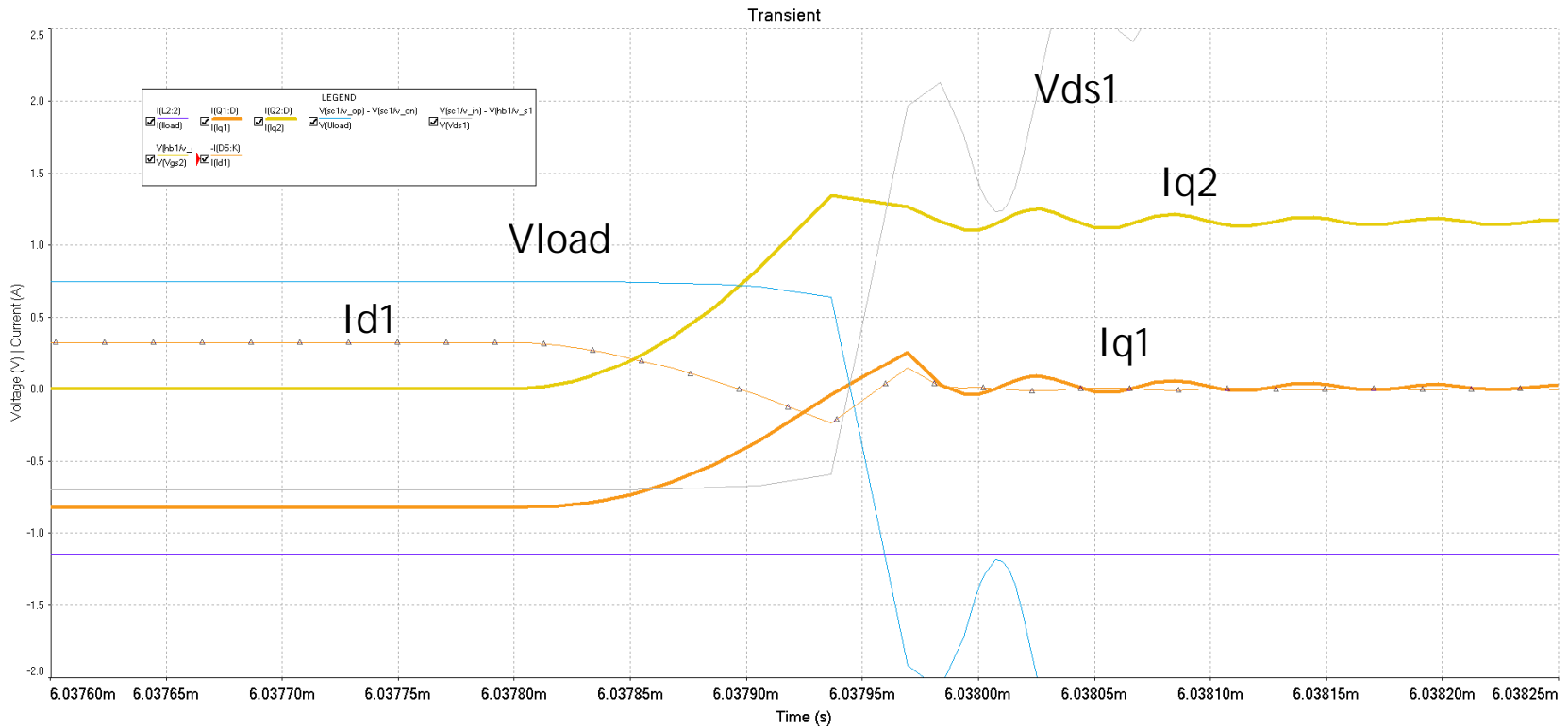
# Zoom in 2: Q2 off – Q1 on



# Zoom in 3: Q2 on



# Zoom in 4: Q2 on





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